

**REFERENCE INFORMATION**
**Table 16-1. -Design notation.**

$A$	cross-sectional area; net bearing area; maximum expected acceleration of bedrock at the site
$A_1$	cross-sectional area of main wood member(s) before boring or grooving
$A_2$	sum of cross-sectional areas of wood or metal side member(s) before boring or drilling
$A_E$	effective bearing area
$A_p$	bearing plate area
$A_s$	cross-sectional area of a steel prestressing rod
$A_v$	cross-sectional area of a transverse glulam deck panel used for determining the magnitude of horizontal shear
$b$	width of rectangular member; bridge width measured between the outside deck edges
$B$	buoyancy
$b_d$	for transverse decks, the wheel load distribution width perpendicular to the deck span
$b_t$	for transverse decks, the wheel load distribution width in the direction of the deck span; for longitudinal decks, the truck tire width perpendicular to traffic
$C$	centrifugal force in percent of live load, combined response coefficient; adjustment factor for railing loads
$C_B$	butt joint factor
$C_C$	curvature factor
$C_D$	duration of load factor
$C_e$	edge-distance factor
$C_F$	size factor
$CF$	centrifugal force
$C_f$	form factor
$C_g$	group action factor
$C_i$	interaction stress factor
$C_k$	for bending members the largest value of the slenderness factor, $C_s$ , at which the intermediate beam equation applies
$C_L$	lateral stability of beams factor
$C_{lb}$	lag screw factor

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Table 16-1. - Design notation (*continued*).

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$C_{LS}$	load-sharing factor
$C_m$	steel dowel bending-stress coefficient
$C_M$	moisture content factor
$C_n$	end-distance factor
$C_p$	lateral stability of columns factor
$C_R$	fire-retardant factor; steel dowel shear-stress coefficient
$C_s$	spacing factor
$C_s$	slenderness factor for bending member
$C_{st}$	steel side-plate factor
$C_t$	temperature factor
$d$	depth of rectangular member; least dimension of rectangular compression member; pennyweight of nail or spike
$D$	dead load; degree of curve; diameter
$d_c$	depth of steel channel
$DL$	uniform dead load of the deck and wearing surface
$D_w$	for longitudinal decks, the wheel load distribution width transverse to the deck span
$e$	eccentricity
$E$	modulus of elasticity; tabulated modulus of elasticity; earth pressure
$E'$	allowable modulus of elasticity
$EQ$	equivalent static horizontal force applied at the center of gravity of the structure; earthquake
$E_{Ts}$	transverse bending modulus of a stress-laminated system
$f_a$	applied stress from axial loading, either tension or compression
$F$	framing factor
$F'_a$	allowable stress from axial loading, either tension or compression
$f_b$	applied bending stress
$F_b$	tabulated bending stress
$F'_b$	allowable bending stress
$F''_b$	intermediate bending stress used to compute $C_k$
$f_c$	applied stress in compression parallel to grain
$F_c$	tabulated stress in compression parallel to grain
$F'_c$	allowable stress in compression parallel to grain
$F''_c$	intermediate stress in compression parallel to grain used to compute $K$
$f_{c\perp}$	applied stress in compression perpendicular to grain

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Table 16-4. - Design notation (*continued*).

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$F_{c\perp}$	tabulated stress in compression perpendicular to grain
$F'_{c\perp}$	allowable stress in compression perpendicular to grain
$f_g$	applied stress in end grain in bearing
$F_g$	tabulated stress for end grain in bearing
$F'_g$	allowable stress for end grain in bearing
$F_L$	longitudinal force transferred to the bridge
$F'_\pi$	allowable stress in compression at an angle to the grain
$F_{ps}$	prestressing force required in a prestressing rod
$f_{pu}$	specified minimum ultimate tensile stress for a prestressing rod
$f_t$	applied stress in tension parallel to grain
$F_t$	tabulated stress in tension parallel to grain
$F'_t$	allowable stress in tension parallel to grain
$f_v$	applied stress in horizontal shear
$F_v$	tabulated stress in horizontal shear
$F'_v$	allowable stress in horizontal shear
$F_y$	minimum specified yield point of steel
$g$	acceleration due to gravity (32.2 ft/sec <sup>2</sup> )
$G$	shear modulus; tabulated shear modulus; specific gravity
$G_{TS}$	transverse shear modulus of a stress-laminated system
$GVW$	gross vehicle weight
$h$	height of the top rail above the reference surface
$I$	moment of inertia; vehicle live load impact factor
$ICE$	ice pressure
$J$	unitless convenience factor for the design of members subjected to combined compression and bending
$K$	minimum value of $\ell/d$ at which a column can be expected to perform as an Euler column; design constant based on the wheel load contact area; a constant for the shape of a pier
$K_e$	effective buckling length factor for columns
$\ell$	unbraced length between points of lateral support along the column length; length of bolt in the main member
$L$	span length of bending member; loaded length of sidewalk; vehicle live load, post spacing
$L_A$	anchorage plate length
$\ell_b$	length of bearing
$\ell_e$	effective span length of bending member; effective length of compression member
$LF$	longitudinal force from vehicle live load

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Table 16-1. - Design notation (*continued*).

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$L_P$	bearing plate length
$l_u$	laterally unsupported span length of a bending member
$M$	bending or resisting moment
MC	moisture content
$M_D$	dowel moment capacity
$M_{DL}$	dead load moment
$M_{DLx}$	primary dead load moment
$M_{LL}$	live load moment
$M_T$	magnitude of transverse bending from applied wheel loads
$M_{WL}$	maximum live load moment produced by one wheel line of the design vehicle
$M_x$	primary live load bending moment
$M_y$	secondary live load bending moment
$n$	number of steel dowels required for each deck span
$N$	applied load on a fastener or fastener group at an angle to the grain; load group number; minimum uniform compressive prestress in service
$N'$	allowable load on a fastener or fastener group at an angle to the grain
$N_i$	level of uniform compressive prestress required at the time of installation
$P$	magnitude of wheel load; magnitude of a concentrated load; magnitude of an axial load; applied or tabulated load parallel to grain on a fastener or fastener group; sidewalk load, stream-flow pressure; total uniform force required to cause a 1-inch maximum horizontal deflection of the structure; highway design load for vehicular railing
$P'$	allowable load parallel to grain on a fastener or fastener group; distributed outward transverse post load for vehicular railing
$P_M$	concentrated lane load for moment
$P'_{MAX}$	maximum allowable load for shear plates loaded parallel to grain
$P_N$	applied or tabulated lateral load for nails and spikes
$P'_N$	allowable lateral load for nails and spikes
$P_V$	concentrated lane load for shear
$P_W$	applied or tabulated fastener load in axial withdrawal
$P'_W$	allowable fastener load in axial withdrawal
$Q$	applied or tabulated load perpendicular to grain on a fastener or fastener group
$Q'$	allowable load perpendicular to grain on a fastener or fastener group

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Table 16-1. - Design notation (*continued*).

$Q'_{MAX}$	maximum allowable load for shear plates loaded perpendicular to grain
$r$	radius of gyration
$R$	reaction or bearing force at the support; radius of curve; rib shortening
$R_D$	dowel shear capacity
$R_{DL}$	dead load reaction
$R_{DLx}$	primary dead load vertical shear
$R_{LL}$	live load reaction
$R_{WL}$	maximum reaction produced by one wheel line of the design vehicle
$R_x$	primary live load vertical shear
$R_y$	secondary live load vertical shear
$s$	effective deck span
$S$	section modulus; beam spacing; design speed; shrinkage
$SF$	stream-flow pressure
$S_p$	center-to-center spacing of prestressing rods
$t$	thickness
$T$	temperature; period of vibration of the structure
$t_p$	bearing plate thickness
$t_w$	steel channel web thickness
$V$	vertical shear force; water velocity
$V_{DL}$	dead load vertical shear
$V_{LD}$	maximum vertical shear produced when wheel lines are laterally distributed as specified for moment
$V_{LL}$	live load vertical shear
$V_{LU}$	maximum vertical shear from an undistributed wheel line
$V_T$	magnitude of transverse shear from applied wheel loads
$V_{WL}$	maximum vertical shear produced by one wheel line of the design vehicle
$w$	magnitude of uniform load; pedestrian or bicycle loading
$W$	total dead load weight of the structure; wind load on structure; vehicle weight; sidewalk width
$W_A$	anchorage plate width
$w_{DL}$	uniform dead load supported by a beam; uniform deck dead load; uniform deck dead load over the wheel load distribution width,
$D_w$	
$WL$	wheel line; wind load on live load

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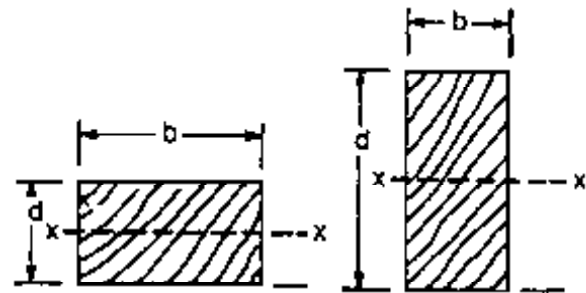
Table 16-1. - Design notation (*continued*).

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$WLF$	the portion of the maximum force or deflection produced by one wheel line that is supported by one longitudinal glulam deck panel
$w_p$	longitudinal glulam panel width in inches
$W_p$	longitudinal glulam panel width in feet; bearing-plate width
$\alpha$	a unitless factor used for determining the wheel load distribution width and magnitude of transverse bending in longitudinal stress-laminated lumber decks
$\beta$	load coefficient (with appropriate subscript); a unitless factor used for determining the magnitude of transverse shear in longitudinal stress-laminated lumber decks
$\gamma$	load factor
$\Delta_{DL}$	dead load deflection
$\Delta_{LL}$	live load deflection
$\Delta_{WL}$	deflection from one wheel line of the design vehicle
$\theta$	angle between the direction of load and direction of grain; a unitless factor used for determining the wheel load distribution width and magnitude of transverse bending in longitudinal stress-laminated lumber decks
$\pi$	pi
$\sigma$	dowel stress from applied loads
$\sigma_A$	allowable dowel stress in bending
$\sigma_{PL}$	proportional limit stress for wood, perpendicular to grain
$\mu$	Poisson's ratio, coefficient of friction
$^{\circ}F$	temperature in degrees fahrenheit
$\varnothing$	diameter
$\leq$	less than or equal to
$<$	less than
$\geq$	greater than or equal to
$>$	greater than

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Table 16-2. - Section properties of structural lumber<sup>a</sup>



Nominal size <i>b</i> x <i>d</i> (in.)	Dressed size <i>b</i> x <i>d</i> (in.)	Area <i>A</i> (in <sup>2</sup> )	<i>S</i> (in <sup>3</sup> )	<i>I</i> (in <sup>4</sup> )	Volume (ft <sup>3</sup> /ft)	Weight <sup>b</sup> (lb/ft)
1 x 3	3/4 x 2-1/2	1.88	0.78	0.98	0.01	0.65
1 x 4	3/4 x 3-1/2	2.63	1.53	2.68	0.02	0.91
1 x 6	3/4 x 5-1/2	4.13	3.78	10.40	0.03	1.43
1 x 8	3/4 x 7-1/4	5.44	6.57	23.82	0.04	1.89
1 x 10	3/4 x 9-1/4	6.94	10.70	49.47	0.05	2.41
1 x 12	3/4 x 11-1/4	8.44	15.82	88.99	0.06	2.93
2 x 3	1-1/2 x 2-1/2	3.75	1.56	1.95	0.03	1.30
2 x 4	1-1/2 x 3-1/2	5.25	3.06	5.36	0.04	1.82
2 x 6	1-1/2 x 5-1/2	8.25	7.56	20.80	0.06	2.86
2 x 8	1-1/2 x 7-1/4	10.88	13.14	47.63	0.08	3.78
2 x 10	1-1/2 x 9-1/4	13.88	21.39	98.93	0.10	4.82
2 x 12	1-1/2 x 11-1/4	16.88	31.64	177.98	0.12	5.86
2 x 14	1-1/2 x 13-1/4	19.88	43.89	290.78	0.14	6.90
3 x 1	2-1/2 x 3/4	1.88	0.23	0.09	0.01	0.65
3 x 2	2-1/2 x 1-1/2	3.75	0.94	0.70	0.03	1.30
3 x 4	2-1/2 x 3-1/2	8.75	5.10	8.93	0.06	3.04
3 x 6	2-1/2 x 5-1/2	13.75	12.60	34.66	0.10	4.77
3 x 8	2-1/2 x 7-1/4	18.13	21.90	79.39	0.13	6.29
3 x 10	2-1/2 x 9-1/4	23.13	35.65	164.89	0.16	8.03
3 x 12	2-1/2 x 11-1/4	28.13	52.73	296.63	0.20	9.77
3 x 14	2-1/2 x 13-1/4	33.13	73.15	484.63	0.23	11.50
3 x 16	2-1/2 x 15-1/4	38.13	96.90	738.87	0.26	13.24
4 x 1	3-1/2 x 3/4	2.63	0.33	0.12	0.02	0.91
4 x 2	3-1/2 x 1-1/2	5.25	1.31	0.98	0.04	1.82
4 x 3	3-1/2 x 2-1/2	8.75	3.65	4.56	0.06	3.04
4 x 4	3-1/2 x 3-1/2	12.25	7.15	12.51	0.09	4.25
4 x 6	3-1/2 x 5-1/2	19.25	17.65	48.53	0.13	6.68
4 x 8	3-1/2 x 7-1/4	25.38	30.66	111.15	0.18	8.81
4 x 10	3-1/2 x 9-1/4	32.38	49.91	230.84	0.22	11.24
4 x 12	3-1/2 x 11-1/4	39.38	73.83	415.28	0.27	13.67
4 x 14	3-1/2 x 13-1/4	46.38	102.41	678.48	0.32	16.09
4 x 16	3-1/2 x 15-1/4	53.38	135.66	1034.42	0.37	18.54
6 x 1	5-1/2 x 3/4	4.13	0.52	0.19	0.03	1.43
6 x 2	5-1/2 x 1-1/2	8.25	2.06	1.55	0.06	2.86
6 x 3	5-1/2 x 2-1/2	13.75	5.73	7.16	0.10	4.77
6 x 4	5-1/2 x 3-1/2	19.25	11.23	19.65	0.13	6.68

<sup>a</sup>Based on dressed (S4S) sizes.

<sup>b</sup>Based on a unit weight of 50 lb/ft<sup>3</sup>.

Table 16-2. - Section properties of structural lumber<sup>a</sup> (continued).

Nominal size b x d (in.)	Dressed size b x d (in.)	Area A (in <sup>2</sup> )	S (in <sup>3</sup> )	I (in <sup>4</sup> )	Volume (ft <sup>3</sup> /ft)	Weight <sup>b</sup> (lb/ft)
6 x 6	5-1/2 x 5-1/2	30.25	27.73	76.26	0.21	10.50
6 x 8	5-1/2 x 7-1/2	41.25	51.56	193.36	0.29	14.32
6 x 10	5-1/2 x 9-1/2	52.25	82.73	392.96	0.36	18.14
6 x 12	5-1/2 x 11-1/2	63.25	121.23	697.07	0.44	21.96
6 x 14	5-1/2 x 13-1/2	74.25	167.06	1,127.67	0.52	25.78
6 x 16	5-1/2 x 15-1/2	85.25	220.23	1,706.78	0.59	29.60
6 x 18	5-1/2 x 17-1/2	96.25	280.73	2,456.38	0.67	33.42
6 x 20	5-1/2 x 19-1/2	107.25	348.56	3,398.48	0.74	37.24
6 x 22	5-1/2 x 21-1/2	118.25	423.73	4,555.09	0.82	41.06
6 x 24	5-1/2 x 23-1/2	129.25	506.23	5,948.19	0.90	44.88
8 x 1	7-1/4 x 3/4	5.44	0.68	0.26	0.05	2.78
8 x 2	7-1/4 x 1-1/2	10.88	2.72	2.04	0.08	3.78
8 x 3	7-1/4 x 2-1/2	18.13	7.55	9.44	0.13	6.29
8 x 4	7-1/4 x 3-1/2	25.38	14.80	25.90	0.18	8.81
8 x 6	7-1/2 x 5-1/2	41.25	37.81	103.98	0.29	14.32
8 x 8	7-1/2 x 7-1/2	56.25	70.31	263.67	0.39	19.53
8 x 10	7-1/2 x 9-1/2	71.25	112.81	535.86	0.49	24.74
8 x 12	7-1/2 x 11-1/2	86.25	165.31	950.55	0.60	29.95
8 x 14	7-1/2 x 13-1/2	101.25	227.81	1,537.73	0.70	35.16
8 x 16	7-1/2 x 15-1/2	116.25	300.31	2,327.42	0.81	40.36
8 x 18	7-1/2 x 17-1/2	131.25	382.81	3,349.61	0.91	45.57
8 x 20	7-1/2 x 19-1/2	146.25	475.31	4,634.30	1.02	50.78
8 x 22	7-1/2 x 21-1/2	161.25	577.81	6,211.48	1.12	55.99
8 x 24	7-1/2 x 23-1/2	176.25	690.31	8,111.17	1.22	61.20
10 x 1	9-1/4 x 3/4	6.94	0.87	0.33	0.05	2.41
10 x 2	9-1/4 x 1-1/2	13.88	3.47	2.60	0.10	4.82
10 x 3	9-1/4 x 2-1/2	23.13	9.64	12.04	0.16	8.03
10 x 4	9-1/4 x 3-1/2	32.38	18.89	33.05	0.22	11.24
10 x 6	9-1/2 x 5-1/2	52.25	47.90	131.71	0.36	18.14
10 x 8	9-1/2 x 7-1/2	71.25	89.06	333.98	0.49	24.74
10 x 10	9-1/2 x 9-1/2	90.25	142.90	678.76	0.63	31.34
10 x 12	9-1/2 x 11-1/2	109.25	209.40	1,204.03	0.76	37.93
10 x 14	9-1/2 x 13-1/2	128.25	288.56	1,947.80	0.89	44.53
10 x 16	9-1/2 x 15-1/2	147.25	380.40	2,948.07	1.02	51.13
10 x 18	9-1/2 x 17-1/2	166.25	484.90	4,242.84	1.15	57.73
10 x 20	9-1/2 x 19-1/2	185.25	602.06	5,870.11	1.29	64.32
10 x 22	9-1/2 x 21-1/2	204.25	731.90	7,867.88	1.42	70.92
10 x 24	9-1/2 x 23-1/2	223.25	874.40	10,274.15	1.55	77.52
12 x 1	11-1/4 x 3/4	8.44	1.05	0.40	0.06	2.93
12 x 2	11-1/4 x 1-1/2	16.88	4.22	3.16	0.12	5.86
12 x 3	11-1/4 x 2-1/2	28.13	11.72	14.65	0.20	9.77
12 x 4	11-1/4 x 3-1/2	39.38	22.97	40.20	0.27	13.67
12 x 6	11-1/2 x 5-1/2	63.25	57.98	159.44	0.44	21.96
12 x 8	11-1/2 x 7-1/2	86.25	107.81	404.30	0.60	29.95
12 x 10	11-1/2 x 9-1/2	109.25	172.98	821.65	0.76	37.93
12 x 12	11-1/2 x 11-1/2	132.25	253.48	1,457.51	0.92	45.92
12 x 14	11-1/2 x 13-1/2	155.25	349.31	2,357.86	1.08	53.91
12 x 16	11-1/2 x 15-1/2	178.25	460.48	3,568.71	1.24	61.89
12 x 18	11-1/2 x 17-1/2	201.25	586.98	5,136.07	1.40	69.88

<sup>a</sup>Based on dressed (S4S) sizes.<sup>b</sup>Based on a unit weight of 50 lb/ft<sup>3</sup>.



Table 16-2. - Section properties of structural lumber<sup>a</sup> (continued).

Nominal size b x d (in.)	Dressed size b x d (in.)	Area A (in <sup>2</sup> )	S (in <sup>3</sup> )	I (in <sup>4</sup> )	Volume (ft <sup>3</sup> /ft)	Weight <sup>b</sup> (lb/ft)
12 x 20	11-1/2 x 19-1/2	224.25	728.81	7,105.92	1.56	77.86
12 x 22	11-1/2 x 21-1/2	247.25	885.98	9,524.28	1.72	85.85
12 x 24	11-1/2 x 23-1/2	270.25	1,058.48	12,437.13	1.88	93.84
14 x 2	13-1/4 x 1-1/2	19.88	4.97	3.73	0.14	6.90
14 x 3	13-1/4 x 2-1/2	33.13	13.80	17.25	0.23	11.50
14 x 4	13-1/2 x 3-1/2	47.25	27.56	48.23	0.33	16.41
14 x 6	13-1/2 x 5-1/2	74.25	68.06	187.17	0.52	25.78
14 x 8	13-1/2 x 7-1/2	101.25	126.56	474.61	0.70	35.16
14 x 10	13-1/2 x 9-1/2	128.25	203.06	964.55	0.89	44.53
14 x 12	13-1/2 x 11-1/2	155.25	297.56	1,710.98	1.08	53.91
14 x 14	13-1/2 x 13-1/2	182.25	410.06	2,767.92	1.27	63.28
14 x 16	13-1/2 x 15-1/2	209.25	540.56	4,189.36	1.45	72.66
14 x 18	13-1/2 x 17-1/2	236.25	689.06	6,029.30	1.64	82.03
14 x 20	13-1/2 x 19-1/2	263.25	855.56	8,341.73	1.83	91.41
14 x 22	13-1/2 x 21-1/2	290.25	1,040.06	11,180.67	2.02	100.78
14 x 24	13-1/2 x 23-1/2	317.25	1,242.56	14,600.11	2.20	110.16
16 x 3	15-1/2 x 2-1/2	38.75	16.15	20.18	0.27	13.45
16 x 4	15-1/2 x 3-1/2	54.25	31.65	55.38	0.38	18.84
16 x 6	15-1/2 x 5-1/2	85.25	78.15	214.90	0.59	29.60
16 x 8	15-1/2 x 7-1/2	116.25	145.31	544.92	0.81	40.36
16 x 10	15-1/2 x 9-1/2	147.25	233.15	1,107.44	1.02	51.13
16 x 12	15-1/2 x 11-1/2	178.25	341.65	1,964.46	1.24	61.89
16 x 14	15-1/2 x 13-1/2	209.25	470.81	3,177.98	1.45	72.66
16 x 16	15-1/2 x 15-1/2	240.25	620.65	4,810.01	1.67	83.42
16 x 18	15-1/2 x 17-1/2	271.25	791.15	6,922.53	1.88	94.18
16 x 20	15-1/2 x 19-1/2	302.25	982.31	9,577.55	2.10	104.95
16 x 22	15-1/2 x 21-1/2	333.25	1,194.15	12,837.07	2.31	115.71
16 x 24	15-1/2 x 23-1/2	364.25	1,426.65	16,763.09	2.53	126.48
18 x 6	17-1/2 x 5-1/2	96.25	88.23	242.63	0.67	33.42
18 x 8	17-1/2 x 7-1/2	131.25	164.06	615.23	0.91	45.57
18 x 10	17-1/2 x 9-1/2	166.25	263.23	1,250.34	1.15	57.73
18 x 12	17-1/2 x 11-1/2	201.25	385.73	2,217.94	1.40	69.88
18 x 14	17-1/2 x 13-1/2	236.25	531.56	3,588.05	1.64	82.03
18 x 16	17-1/2 x 15-1/2	271.25	700.73	5,430.65	1.88	94.18
18 x 18	17-1/2 x 17-1/2	306.25	893.23	7,815.76	2.13	106.34
18 x 20	17-1/2 x 19-1/2	341.25	1,109.06	10,813.36	2.37	118.49
18 x 22	17-1/2 x 21-1/2	376.25	1,348.23	14,493.46	2.61	130.64
18 x 24	17-1/2 x 23-1/2	411.25	1,610.73	18,926.07	2.86	142.80
20 x 6	19-1/2 x 5-1/2	107.25	98.31	270.36	0.74	37.24
20 x 8	19-1/2 x 7-1/2	146.25	182.81	685.55	1.02	50.78
20 x 10	19-1/2 x 9-1/2	185.25	293.31	1,393.23	1.29	64.32
20 x 12	19-1/2 x 11-1/2	224.25	429.81	2,471.42	1.56	77.86
20 x 14	19-1/2 x 13-1/2	263.25	592.31	3,998.11	1.83	91.41
20 x 16	19-1/2 x 15-1/2	302.25	780.81	6,051.30	2.10	104.95
20 x 18	19-1/2 x 17-1/2	341.25	995.31	8,708.98	2.37	118.49
20 x 20	19-1/2 x 19-1/2	380.25	1,235.81	12,049.17	2.64	132.03
20 x 22	19-1/2 x 21-1/2	419.25	1,502.31	16,149.86	2.91	145.57
20 x 24	19-1/2 x 23-1/2	458.25	1,794.81	21,089.05	3.18	159.11

<sup>a</sup>Based on dressed (S4S) sizes.<sup>b</sup>Based on a unit weight of 50 lb/ft<sup>3</sup>.

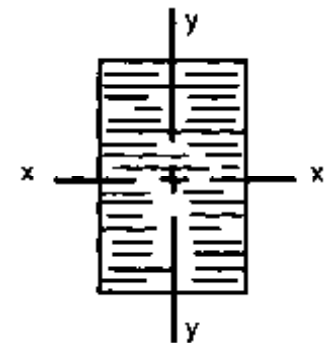
Table 16-2. - Section properties of structural lumber<sup>a</sup> (continued).

Nominal size <i>b x d</i> (in.)	Dressed size <i>b x d</i> (in.)	Area <i>A</i> (in <sup>2</sup> )	<i>S</i> (in <sup>3</sup> )	<i>I</i> (in <sup>4</sup> )	Volume (ft <sup>3</sup> /ft)	Weight <sup>b</sup> (lb/ft)
22 x 6	21-1/2 x 5-1/2	118.25	108.40	298.09	0.82	41.06
22 x 8	21-1/2 x 7-1/2	161.25	201.56	755.86	1.12	55.99
22 x 10	21-1/2 x 9-1/2	204.25	323.40	1,536.13	1.42	70.92
22 x 12	21-1/2 x 11-1/2	247.25	473.90	2,724.90	1.72	85.85
22 x 14	21-1/2 x 13-1/2	290.25	653.06	4,408.17	2.02	100.78
22 x 16	21-1/2 x 15-1/2	333.25	860.90	6,671.94	2.31	115.71
22 x 18	21-1/2 x 17-1/2	376.25	1,097.40	9,602.21	2.61	130.64
22 x 20	21-1/2 x 19-1/2	419.25	1,362.56	13,284.98	2.91	145.57
22 x 22	21-1/2 x 21-1/2	462.25	1,656.40	17,806.26	3.21	160.50
22 x 24	21-1/2 x 23-1/2	505.25	1,978.90	23,252.03	3.51	175.43
24 x 6	23-1/2 x 5-1/2	129.25	118.48	325.82	0.90	44.88
24 x 8	23-1/2 x 7-1/2	176.25	220.31	826.17	1.22	61.20
24 x 10	23-1/2 x 9-1/2	223.25	353.48	1,679.03	1.55	77.52
24 x 12	23-1/2 x 11-1/2	270.25	517.98	2,978.38	1.88	93.84
24 x 14	23-1/2 x 13-1/2	317.25	713.81	4,818.23	2.20	110.16
24 x 16	23-1/2 x 15-1/2	364.25	940.98	7,292.59	2.53	126.48
24 x 18	23-1/2 x 17-1/2	411.25	1,199.48	10,495.44	2.86	142.80
24 x 20	23-1/2 x 19-1/2	458.25	1,489.31	14,520.80	3.18	159.11
24 x 22	23-1/2 x 21-1/2	505.25	1,810.48	19,462.65	3.51	175.43
24 x 24	23-1/2 x 23-1/2	552.25	2,162.98	25,415.01	3.84	191.75

<sup>a</sup> Based on dressed (S4S) sizes.

<sup>b</sup> Based on a unit weight of 50 lb/ft<sup>3</sup>.

Table 16-3. - Section properties for structural glulam manufactured from western species with 1-1/2-inch-thick laminations.



Depth <i>d</i> (In.)	Size factor <i>C<sub>F</sub></i>	Area <i>A</i> (in <sup>2</sup> )	<i>X-X axis</i>			<i>Y-Y axis</i>		Volume (ft <sup>3</sup> /ft)	Weight <sup>a</sup> (lb/ft)
			<i>S<sub>x</sub></i> (in <sup>3</sup> )	<i>S<sub>x</sub>C<sub>F</sub></i> (in <sup>3</sup> )	<i>I<sub>x</sub></i> (in <sup>4</sup> )	<i>S<sub>y</sub></i> (in <sup>3</sup> )	<i>I<sub>y</sub></i> (in <sup>4</sup> )		
3-1/8 inch width									
3	1.00	9.4	4.7	4.7	7.0	4.9	7.6	0.07	3.3
4-1/2	1.00	14.1	10.5	10.5	23.7	7.3	11.4	0.10	4.9
6	1.00	18.8	18.8	18.8	56.3	9.8	15.3	0.13	6.5
7-1/2	1.00	23.4	29.3	29.3	109.9	12.2	19.1	0.16	8.1
9	1.00	28.1	42.2	42.2	189.8	14.6	22.9	0.20	9.8
10-1/2	1.00	32.8	57.4	57.4	301.5	17.1	26.7	0.23	11.4
12	1.00	37.5	75.0	75.0	450.0	19.5	30.5	0.26	13.0
13-1/2	0.99	42.2	94.9	93.7	640.7	22.0	34.3	0.29	14.6
15	0.98	46.9	117.2	114.3	878.9	24.4	38.1	0.33	16.3
16-1/2	0.97	51.6	141.8	136.9	1,169.8	26.9	42.0	0.36	17.9
18	0.96	56.3	168.8	161.3	1,518.8	29.3	45.8	0.39	19.5
19-1/2	0.95	60.9	198.0	187.6	1,931.0	31.7	49.6	0.42	21.2
21	0.94	65.6	229.7	215.8	2,411.7	34.2	53.4	0.46	22.8
22-1/2	0.93	70.3	263.7	245.9	2,966.3	36.6	57.2	0.49	24.4
24	0.93	75.0	300.0	277.8	3,600.0	39.1	61.0	0.52	26.0
25-1/2	0.92	79.7	338.7	311.5	4,318.1	41.5	64.8	0.55	27.7
27	0.91	84.4	379.7	347.0	5,125.8	43.9	68.7	0.59	29.3
28-1/2	0.91	89.1	423.0	384.3	6,028.4	46.4	72.5	0.62	30.9
30	0.90	93.8	468.8	423.4	7,031.3	48.8	76.3	0.65	32.6
5-1/8-inch width									
3	1.00	15.4	7.7	7.7	11.5	13.1	33.7	0.11	5.3
4-1/2	1.00	23.1	17.3	17.3	38.9	19.7	50.5	0.16	8.0
6	1.00	30.8	30.8	30.8	92.3	26.3	67.3	0.21	10.7
7-1/2	1.00	38.4	48.0	48.0	180.2	32.8	84.1	0.27	13.3
9	1.00	46.1	69.2	69.2	311.3	39.4	101.0	0.32	16.0
10-1/2	1.00	53.8	94.2	94.2	494.4	46.0	117.8	0.37	18.7
12	1.00	61.5	123.0	123.0	738.0	52.5	134.6	0.43	21.4
13-1/2	0.99	69.2	155.7	153.6	1,050.8	59.1	151.4	0.48	24.0
15	0.98	76.9	192.2	187.5	1,441.4	65.7	168.3	0.53	26.7
16-1/2	0.97	84.6	232.5	224.5	1,918.5	72.2	185.1	0.59	29.4
18	0.96	92.3	276.8	264.6	2,490.8	78.8	201.9	0.64	32.0

<sup>a</sup>Based on a unit weight of 50 lb/ft<sup>3</sup>.

Table 16-3. - Section properties for structural glulam manufactured from western species with 1-1/2-inch-thick laminations (*continued*).

Depth <i>d</i> (in.)	Size factor <i>C<sub>F</sub></i>	Area <i>A</i> (in <sup>2</sup> )	<i>X-X axis</i>			<i>Y-Y axis</i>		Volume (ft <sup>3</sup> /ft)	Weight <sup>a</sup> (lb/ft)
			<i>S<sub>x</sub></i> (in <sup>3</sup> )	<i>S<sub>x</sub>C<sub>F</sub></i> (in <sup>3</sup> )	<i>I<sub>x</sub></i> (in <sup>4</sup> )	<i>S<sub>y</sub></i> (in <sup>3</sup> )	<i>I<sub>y</sub></i> (in <sup>4</sup> )		
5-1/8-inch width (continued)									
19-1/2	0.95	99.9	324.8	307.7	3,166.8	85.4	218.7	0.69	34.7
21	0.94	107.6	376.7	354.0	3,955.2	91.9	235.6	0.75	37.4
22-1/2	0.93	115.3	432.4	403.3	4,864.7	98.5	252.4	0.80	40.0
24	0.93	123.0	492.0	455.5	5,904.0	105.1	269.2	0.85	42.7
25-1/2	0.92	130.7	555.4	510.8	7,081.6	111.6	286.0	0.91	45.4
27	0.91	138.4	622.7	569.0	8,406.3	118.2	302.9	0.96	48.0
28-1/2	0.91	146.1	693.8	630.2	9,886.6	124.8	319.7	1.01	50.7
30	0.90	153.8	768.8	694.3	11,531.3	131.3	336.5	1.07	53.4
31-1/2	0.90	161.4	847.5	761.4	13,348.9	137.9	353.4	1.12	56.1
33	0.89	169.1	930.2	831.3	15,348.1	144.5	370.2	1.17	58.7
34-1/2	0.89	176.8	1,016.7	904.1	17,537.6	151.0	387.0	1.23	61.4
36	0.89	184.5	1,107.0	979.8	19,926.0	157.6	403.8	1.28	64.1
6-3/4-inch width									
6	1.00	40.5	40.5	40.5	121.5	45.6	153.8	0.28	14.1
7-1/2	1.00	50.6	63.3	63.3	237.3	57.0	192.2	0.35	17.6
9	1.00	60.8	91.1	91.1	410.1	68.3	230.7	0.42	21.1
10-1/2	1.00	70.9	124.0	124.0	651.2	79.7	269.1	0.49	24.6
12	1.00	81.0	162.0	162.0	972.0	91.1	307.5	0.56	28.1
13-1/2	0.99	91.1	205.0	202.4	1,384.0	102.5	346.0	0.63	31.6
15	0.98	101.3	253.1	246.9	1,898.4	113.9	384.4	0.70	35.2
16-1/2	0.97	111.4	306.3	295.6	2,526.8	125.3	422.9	0.77	38.7
18	0.96	121.5	364.5	348.4	3,280.5	136.7	461.3	0.84	42.2
19-1/2	0.95	131.6	427.8	405.3	4,170.9	148.1	499.8	0.91	45.7
21	0.94	141.8	496.1	466.2	5,209.3	159.5	538.2	0.98	49.2
22-1/2	0.93	151.9	569.5	531.1	6,407.2	170.9	576.7	1.05	52.7
24	0.93	162.0	648.0	600.0	7,776.0	182.3	615.1	1.13	56.3
25-1/2	0.92	172.1	731.5	672.8	9,327.0	193.6	653.5	1.20	59.8
27	0.91	182.3	820.1	749.5	11,071.7	205.0	692.0	1.27	63.3
28-1/2	0.91	192.4	913.8	830.1	13,021.4	216.4	730.4	1.34	66.8
30	0.90	202.5	1,012.5	914.5	15,187.5	227.8	768.9	1.41	70.3
31-1/2	0.90	212.6	1,116.3	1,002.8	17,581.4	239.2	807.3	1.48	73.8
33	0.89	222.8	1,225.1	1,094.9	20,214.6	250.6	845.8	1.55	77.3
34-1/2	0.89	232.9	1,339.0	1,190.8	23,098.3	262.0	884.2	1.62	80.9
36	0.89	243.0	1,458.0	1,290.5	26,244.0	273.4	922.6	1.69	84.4
37-1/2	0.88	253.1	1,582.0	1,393.9	29,663.1	284.8	961.1	1.76	87.9
39	0.88	263.3	1,711.1	1,501.1	33,366.9	296.2	999.5	1.83	91.4
40-1/2	0.87	273.4	1,845.3	1,612.0	37,366.9	307.5	1,038.0	1.90	94.9
42	0.87	283.5	1,984.5	1,726.7	41,674.5	318.9	1,076.4	1.97	98.4
43-1/2	0.87	293.6	2,128.8	1,845.0	46,301.0	330.3	1,114.9	2.04	102.0
45	0.86	303.8	2,278.1	1,967.0	51,257.8	341.7	1,153.3	2.11	105.5
46-1/2	0.86	313.9	2,432.5	2,092.7	56,556.4	353.1	1,191.7	2.18	109.0
48	0.86	324.0	2,592.0	2,222.0	62,208.0	364.5	1,230.2	2.25	112.5

<sup>a</sup>Based on a unit weight of 50 lb/ft<sup>3</sup>.

Table 16-3. - Section properties for structural glulam manufactured from western species with 1-1/2-inch-thick laminations (*continued*).

Depth <i>d</i> (In.)	Size factor <i>C<sub>F</sub></i>	Area <i>A</i> (in <sup>2</sup> )	X-X axis			Y-Y axis		Volume (ft <sup>3</sup> /ft)	Weight <sup>a</sup> (lb/ft)
			<i>S<sub>x</sub></i> (in <sup>3</sup> )	<i>S<sub>x</sub>C<sub>F</sub></i> (in <sup>3</sup> )	<i>I<sub>x</sub></i> (in <sup>4</sup> )	<i>S<sub>y</sub></i> (in <sup>3</sup> )	<i>I<sub>y</sub></i> (in <sup>4</sup> )		
8-3/4-inch width									
7-1/2	1.00	65.6	82.0	82.0	307.6	95.7	418.7	0.46	22.8
9	1.00	78.8	118.1	118.1	531.6	114.8	502.4	0.55	27.3
10-1/2	1.00	91.9	160.8	160.8	844.1	134.0	586.2	0.64	31.9
12	1.00	105.0	210.0	210.0	1,260.0	153.1	669.9	0.73	36.5
13-1/2	0.99	118.1	265.8	262.3	1,794.0	172.3	753.7	0.82	41.0
15	0.98	131.3	328.1	320.1	2,460.9	191.4	837.4	0.91	45.6
16-1/2	0.97	144.4	397.0	383.2	3,275.5	210.5	921.1	1.00	50.1
18	0.96	157.5	472.5	451.7	4,252.5	229.7	1,004.9	1.09	54.7
19-1/2	0.95	170.6	554.5	525.4	5,406.7	248.8	1,088.6	1.18	59.2
21	0.94	183.8	643.1	604.4	6,752.8	268.0	1,172.4	1.28	63.8
22-1/2	0.93	196.9	738.3	688.5	8,305.7	287.1	1,256.1	1.37	68.4
24	0.93	210.0	840.0	777.7	10,080.0	306.3	1,339.8	1.46	72.9
25-1/2	0.92	223.1	948.3	872.1	12,090.6	325.4	1,423.6	1.55	77.5
27	0.91	236.3	1,063.1	971.5	14,352.2	344.5	1,507.3	1.64	82.0
28-1/2	0.91	249.4	1,184.5	1,076.0	16,879.6	363.7	1,591.1	1.73	86.6
30	0.90	262.5	1,312.5	1,185.5	19,687.5	382.8	1,674.8	1.82	91.1
31-1/2	0.90	275.6	1,447.0	1,299.9	22,790.7	402.0	1,758.5	1.91	95.7
33	0.89	288.8	1,588.1	1,419.3	26,204.1	421.1	1,842.3	2.01	100.3
34-1/2	0.89	301.9	1,735.8	1,543.6	29,942.2	440.2	1,926.0	2.10	104.8
36	0.89	315.0	1,890.0	1,672.8	34,020.0	459.4	2,009.8	2.19	109.4
37-1/2	0.88	328.1	2,050.8	1,806.9	38,452.1	478.5	2,093.5	2.28	113.9
39	0.88	341.3	2,218.1	1,945.9	43,253.4	497.7	2,177.2	2.37	118.5
40-1/2	0.87	354.4	2,392.0	2,089.7	48,438.6	516.8	2,261.0	2.46	123.0
42	0.87	367.5	2,572.5	2,238.3	54,022.5	535.9	2,344.7	2.55	127.6
43-1/2	0.87	380.6	2,759.5	2,391.6	60,019.8	555.1	2,428.5	2.64	132.2
45	0.86	393.8	2,953.1	2,549.8	66,445.3	574.2	2,512.2	2.73	136.7
46-1/2	0.86	406.9	3,153.3	2,712.7	73,313.8	593.4	2,595.9	2.83	141.3
48	0.86	420.0	3,360.0	2,880.4	80,640.0	612.5	2,679.7	2.92	145.8
49-1/2	0.85	433.1	3,573.3	3,052.8	88,438.7	631.6	2,763.4	3.01	150.4
51	0.85	446.3	3,793.1	3,229.9	96,724.7	650.8	2,847.2	3.10	154.9
52-1/2	0.85	459.4	4,019.5	3,411.6	105,512.7	669.9	2,930.9	3.19	159.5
54	0.85	472.5	4,252.5	3,598.1	114,817.5	689.1	3,014.6	3.28	164.1
55-1/2	0.84	485.6	4,492.0	3,789.2	124,653.9	708.2	3,098.4	3.37	168.6
57	0.84	498.8	4,738.1	3,985.0	135,036.6	727.3	3,182.1	3.46	173.2
58-1/2	0.84	511.9	4,990.8	4,185.4	145,980.4	746.5	3,265.9	3.55	177.7
60	0.84	525.0	5,250.0	4,390.4	157,500.0	765.6	3,349.6	3.65	182.3
61-1/2	0.83	538.1	5,515.8	4,600.0	169,610.3	784.8	3,433.3	3.74	186.8
10-3/4-inch width									
10-1/2	1.00	112.9	197.5	197.5	1,037.0	202.2	1,087.0	0.78	39.2
12	1.00	129.0	258.0	258.0	1,548.0	231.1	1,242.3	0.90	44.8
13-1/2	0.99	145.1	326.5	322.3	2,204.1	260.0	1,397.6	1.01	50.4
15	0.98	161.3	403.1	393.3	3,023.4	288.9	1,552.9	1.12	56.0
16-1/2	0.97	177.4	487.8	470.8	4,024.2	317.8	1,708.2	1.23	61.6

<sup>a</sup>Based on a unit weight of 50 lb/ft<sup>3</sup>.

Table 16-3. - Section properties for structural glulam manufactured from western species with 1-1/2-inch-thick laminations (*continued*).

Depth <i>d</i> (In.)	Size factor <i>C<sub>F</sub></i>	Area <i>A</i> (in <sup>2</sup> )	X-X axis			Y-Y axis		Volume (ft <sup>3</sup> /ft)	Weight <sup>a</sup> (lb/ft)
			<i>S<sub>x</sub></i> (In <sup>3</sup> )	<i>S<sub>x</sub>C<sub>F</sub></i> (in <sup>3</sup> )	<i>I<sub>x</sub></i> (In <sup>4</sup> )	<i>S<sub>y</sub></i> (In <sup>3</sup> )	<i>I<sub>y</sub></i> (In <sup>4</sup> )		
10-3/4-inch width (continued)									
18	0.96	193.5	580.5	554.9	5,224.5	346.7	1,863.4	1.34	67.2
19-1/2	0.95	209.6	681.3	645.5	6,642.5	375.6	2,018.7	1.46	72.8
21	0.94	225.8	790.1	742.5	8,296.3	404.5	2,174.0	1.57	78.4
22-1/2	0.93	241.9	907.0	845.8	10,204.1	433.4	2,329.3	1.68	84.0
24	0.93	258.0	1,032.0	955.5	12,384.0	462.3	2,484.6	1.79	89.6
25-1/2	0.92	274.1	1,165.0	1,071.4	14,854.1	491.1	2,639.9	1.90	95.2
27	0.91	290.3	1,306.1	1,193.6	17,632.7	520.0	2,795.2	2.02	100.8
28-1/2	0.91	306.4	1,455.3	1,321.9	20,737.8	548.9	2,950.5	2.13	106.4
30	0.90	322.5	1,612.5	1,456.4	24,187.5	577.8	3,105.7	2.24	112.0
31-1/2	0.90	338.6	1,777.8	1,597.0	28,000.1	606.7	3,261.0	2.35	117.6
33	0.89	354.8	1,951.1	1,743.7	32,193.6	635.6	3,416.3	2.46	123.2
34-1/2	0.89	370.9	2,132.5	1,896.4	36,786.2	664.5	3,571.6	2.58	128.8
36	0.89	387.0	2,322.0	2,055.2	41,796.0	693.4	3,726.9	2.69	134.4
37-1/2	0.88	403.1	2,519.5	2,219.9	47,241.2	722.3	3,882.2	2.80	140.0
39	0.88	419.3	2,725.1	2,390.7	53,139.9	751.2	4,037.5	2.91	145.6
40-1/2	0.87	435.4	2,938.8	2,567.3	59,510.3	780.0	4,192.8	3.02	151.2
42	0.87	451.5	3,160.5	2,749.9	66,370.5	808.9	4,348.0	3.14	156.8
43-1/2	0.87	467.6	3,390.3	2,938.3	73,738.6	837.8	4,503.3	3.25	162.4
45	0.86	483.8	3,628.1	3,132.6	81,632.8	866.7	4,658.6	3.36	168.0
46-1/2	0.86	499.9	3,874.0	3,332.8	90,071.2	895.6	4,813.9	3.47	173.6
48	0.86	516.0	4,128.0	3,538.8	99,072.0	924.5	4,969.2	3.58	179.2
49-1/2	0.85	532.1	4,390.0	3,750.5	108,653.3	953.4	5,124.5	3.70	184.8
51	0.85	548.3	4,660.1	3,968.1	118,833.2	982.3	5,279.8	3.81	190.4
52-1/2	0.85	564.4	4,938.3	4,191.4	129,629.9	1,011.2	5,435.0	3.92	196.0
54	0.85	580.5	5,224.5	4,420.5	141,061.5	1,040.1	5,590.3	4.03	201.6
55-1/2	0.84	596.6	5,518.8	4,655.3	153,146.2	1,069.0	5,745.6	4.14	207.2
57	0.84	612.8	5,821.1	4,895.8	165,902.1	1,097.8	5,900.9	4.26	212.8
58-1/2	0.84	628.9	6,131.5	5,142.0	179,347.3	1,126.7	6,056.2	4.37	218.4
60	0.84	645.0	6,450.0	5,393.9	193,500.0	1,155.6	6,211.5	4.48	224.0
61-1/2	0.83	661.1	6,776.5	5,651.5	208,378.3	1,184.5	6,366.8	4.59	229.6
63	0.83	677.3	7,111.1	5,914.6	224,000.4	1,213.4	6,522.1	4.70	235.2
64-1/2	0.83	693.4	7,453.8	6,183.5	240,384.4	1,242.3	6,677.3	4.82	240.8
66	0.83	709.5	7,804.5	6,457.9	257,548.5	1,271.2	6,832.6	4.93	246.4
67-1/2	0.83	725.6	8,163.3	6,737.9	275,510.7	1,300.1	6,987.9	5.04	252.0
69	0.82	741.8	8,530.1	7,023.5	294,289.3	1,329.0	7,143.2	5.15	257.6
70-1/2	0.82	757.9	8,905.0	7,314.7	313,902.4	1,357.9	7,298.5	5.26	263.2
72	0.82	774.0	9,288.0	7,611.5	334,368.0	1,386.8	7,453.8	5.38	268.8
73-1/2	0.82	790.1	9,679.0	7,913.8	355,704.4	1,415.6	7,609.1	5.49	274.3
75	0.82	806.3	10,078.1	8,221.6	377,929.7	1,444.5	7,764.4	5.60	279.9
12-1/4-inch width									
12	1.00	147.0	294.0	294.0	1,764.0	300.1	1,838.3	1.02	51.0
13-1/2	0.99	165.4	372.1	367.3	2,511.6	337.6	2,068.0	1.15	57.4
15	0.98	183.8	459.4	448.1	3,445.3	375.2	2,297.8	1.28	63.8
16-1/2	0.97	202.1	555.8	536.5	4,585.7	412.7	2,527.6	1.40	70.2

<sup>a</sup>Based on a unit weight of 50 lb/ft<sup>3</sup>.

Table 16-3. - Section properties for structural glulam manufactured from western species with 1-1/2-inch-thick laminations (*continued*).

Depth <i>d</i> (in.)	Size factor <i>C<sub>F</sub></i>	Area <i>A</i> (in <sup>2</sup> )	X-X axis			Y-Y axis		Volume (ft <sup>3</sup> /ft)	Weight <sup>a</sup> (lb/ft)
			<i>S<sub>x</sub></i> (in <sup>3</sup> )	<i>S<sub>x</sub>C<sub>F</sub></i> (in <sup>3</sup> )	<i>I<sub>x</sub></i> (in <sup>4</sup> )	<i>S<sub>y</sub></i> (in <sup>3</sup> )	<i>I<sub>y</sub></i> (in <sup>4</sup> )		
12-1/4-inch width (continued)									
18	0.96	220.5	661.5	632.4	5,953.5	450.2	2,757.4	1.53	76.6
19-1/2	0.95	238.9	776.3	735.6	7,569.4	487.7	2,987.2	1.66	82.9
21	0.94	257.3	900.4	846.1	9,453.9	525.2	3,217.0	1.79	89.3
22-1/2	0.93	275.6	1,033.6	963.9	11,627.9	562.7	3,446.7	1.91	95.7
24	0.93	294.0	1,176.0	1,088.8	14,112.0	600.3	3,676.5	2.04	102.1
25-1/2	0.92	312.4	1,327.6	1,220.9	16,926.8	637.8	3,906.3	2.17	108.5
27	0.91	330.8	1,488.4	1,360.1	20,093.1	675.3	4,136.1	2.30	114.8
28-1/2	0.91	349.1	1,658.3	1,506.4	23,631.4	712.8	4,365.9	2.42	121.2
30	0.90	367.5	1,837.5	1,659.6	27,562.5	750.3	4,595.7	2.55	127.6
31-1/2	0.90	385.9	2,025.8	1,819.9	31,907.0	787.8	4,825.4	2.68	134.0
33	0.89	404.3	2,223.4	1,987.0	36,685.7	825.3	5,055.2	2.81	140.4
34-1/2	0.89	422.6	2,430.1	2,161.1	41,919.1	862.9	5,285.0	2.93	146.7
36	0.89	441.0	2,646.0	2,342.0	47,628.0	900.4	5,514.8	3.06	153.1
37-1/2	0.88	459.4	2,871.1	2,529.7	53,833.0	937.9	5,744.6	3.19	159.5
39	0.88	477.8	3,105.4	2,724.2	60,554.8	975.4	5,974.4	3.32	165.9
40-1/2	0.87	496.1	3,348.8	2,925.5	67,814.1	1,012.9	6,204.1	3.45	172.3
42	0.87	514.5	3,601.5	3,133.6	75,631.5	1,050.4	6,433.9	3.57	178.6
43-1/2	0.87	532.9	3,863.3	3,348.3	84,027.7	1,088.0	6,663.7	3.70	185.0
45	0.86	551.3	4,134.4	3,569.7	93,023.4	1,125.5	6,893.5	3.83	191.4
46-1/2	0.86	569.6	4,414.6	3,797.8	102,639.3	1,163.0	7,123.3	3.96	197.8
48	0.86	588.0	4,704.0	4,032.5	112,896.0	1,200.5	7,353.1	4.08	204.2
49-1/2	0.85	606.4	5,002.6	4,273.9	123,814.2	1,238.0	7,582.8	4.21	210.5
51	0.85	624.8	5,310.4	4,521.8	135,414.6	1,275.5	7,812.6	4.34	216.9
52-1/2	0.85	643.1	5,627.3	4,776.3	147,717.8	1,313.0	8,042.4	4.47	223.3
54	0.85	661.5	5,953.5	5,037.3	160,744.5	1,350.6	8,272.2	4.59	229.7
55-1/2	0.84	679.9	6,288.8	5,304.9	174,515.4	1,388.1	8,502.0	4.72	236.1
57	0.84	698.3	6,633.4	5,579.0	189,051.2	1,425.6	8,731.8	4.85	242.4
58-1/2	0.84	716.6	6,987.1	5,859.5	204,372.5	1,463.1	8,961.5	4.98	248.8
60	0.84	735.0	7,350.0	6,146.6	220,500.0	1,500.6	9,191.3	5.10	255.2
61-1/2	0.83	753.4	7,722.1	6,440.0	237,454.4	1,538.1	9,421.1	5.23	261.6
63	0.83	771.8	8,103.4	6,739.9	255,256.3	1,575.7	9,650.9	5.36	268.0
64-1/2	0.83	790.1	8,493.8	7,046.3	273,926.5	1,613.2	9,880.7	5.49	274.3
66	0.83	808.5	8,893.5	7,359.0	293,485.5	1,650.7	10,110.5	5.61	280.7
67-1/2	0.83	826.9	9,302.3	7,678.1	313,954.1	1,688.2	10,340.2	5.74	287.1
69	0.82	845.3	9,720.4	8,003.6	335,352.9	1,725.7	10,570.0	5.87	293.5
70-1/2	0.82	863.6	10,147.6	8,335.4	357,702.7	1,763.2	10,799.8	6.00	299.9
72	0.82	882.0	10,584.0	8,673.6	381,024.0	1,800.8	11,029.6	6.13	306.3
73-1/2	0.82	900.4	11,029.6	9,018.0	405,337.6	1,838.3	11,259.4	6.25	312.6
75	0.82	918.8	11,484.4	9,368.8	430,664.1	1,875.8	11,489.2	6.38	319.0
76-1/2	0.81	937.1	11,948.3	9,725.9	457,024.1	1,913.3	11,718.9	6.51	325.4
78	0.81	955.5	12,421.5	10,089.3	484,438.5	1,950.8	11,948.7	6.64	331.8
79-1/2	0.81	973.9	12,903.8	10,458.9	512,927.8	1,988.3	12,178.5	6.76	338.2
81	0.81	992.3	13,395.4	10,834.8	542,512.7	2,025.8	12,408.3	6.89	344.5
82-1/2	0.81	1,010.6	13,896.1	11,216.9	573,213.9	2,063.4	12,638.1	7.02	350.9
84	0.81	1,029.0	14,406.0	11,605.2	605,052.0	2,100.9	12,867.9	7.15	357.3

<sup>a</sup> Based on a unit weight of 50 lb/ft<sup>3</sup>.

Table 16-3. - Section properties for structural glulam manufactured from western species with 1-1/2-inch-thick laminations (*continued*).

Depth <i>d</i> (In.)	Size factor <i>C<sub>F</sub></i>	Area <i>A</i> (in <sup>2</sup> )	X-X axis			Y-Y axis		Volume (ft <sup>3</sup> /ft)	Weight <sup>a</sup> (lb/ft)
			<i>S<sub>x</sub></i> (in <sup>3</sup> )	<i>S<sub>x</sub>C<sub>F</sub></i> (in <sup>3</sup> )	<i>I<sub>x</sub></i> (in <sup>4</sup> )	<i>S<sub>y</sub></i> (in <sup>3</sup> )	<i>I<sub>y</sub></i> (in <sup>4</sup> )		
14-1/4-inch width									
13-1/2	0.99	192.4	432.8	427.2	2,921.7	456.9	3,255.3	1.34	66.8
15	0.98	213.8	534.4	521.3	4,007.8	507.7	3,617.1	1.48	74.2
16-1/2	0.97	235.1	646.6	624.1	5,334.4	558.4	3,978.8	1.63	81.6
18	0.96	256.5	769.5	735.6	6,925.5	609.2	4,340.5	1.78	89.1
19-1/2	0.95	277.9	903.1	855.7	8,805.2	660.0	4,702.2	1.93	96.5
21	0.94	299.3	1,047.4	984.2	10,997.4	710.7	5,063.9	2.08	103.9
22-1/2	0.93	320.6	1,202.3	1,121.2	13,526.4	761.5	5,425.6	2.23	111.3
24	0.93	342.0	1,368.0	1,266.6	16,416.0	812.3	5,787.3	2.38	118.8
25-1/2	0.92	363.4	1,544.3	1,420.3	19,690.4	863.0	6,149.0	2.52	126.2
27	0.91	384.8	1,731.4	1,582.2	23,373.6	913.8	6,510.7	2.67	133.6
28-1/2	0.91	406.1	1,929.1	1,752.3	27,489.6	964.5	6,872.4	2.82	141.0
30	0.90	427.5	2,137.5	1,930.6	32,062.5	1,015.3	7,234.1	2.97	148.4
31-1/2	0.90	448.9	2,356.6	2,117.0	37,116.4	1,066.1	7,595.8	3.12	155.9
33	0.89	470.3	2,586.4	2,311.4	42,675.2	1,116.8	7,957.5	3.27	163.3
34-1/2	0.89	491.6	2,826.8	2,513.9	48,763.1	1,167.6	8,319.2	3.41	170.7
36	0.89	513.0	3,078.0	2,724.3	55,404.0	1,218.4	8,680.9	3.56	178.1
37-1/2	0.88	534.4	3,339.8	2,942.7	62,622.1	1,269.1	9,042.6	3.71	185.5
39	0.88	555.8	3,612.4	3,169.0	70,441.3	1,319.9	9,404.3	3.86	193.0
40-1/2	0.87	577.1	3,895.6	3,403.2	78,885.8	1,370.7	9,766.0	4.01	200.4
42	0.87	598.5	4,189.5	3,645.2	87,979.5	1,421.4	10,127.7	4.16	207.8
43-1/2	0.87	619.9	4,494.1	3,895.0	97,746.5	1,472.2	10,489.4	4.30	215.2
45	0.86	641.3	4,809.4	4,152.5	108,210.9	1,523.0	10,851.2	4.45	222.7
46-1/2	0.86	662.6	5,135.3	4,417.9	119,396.7	1,573.7	11,212.9	4.60	230.1
48	0.86	684.0	5,472.0	4,690.9	131,328.0	1,624.5	11,574.6	4.75	237.5
49-1/2	0.85	705.4	5,819.3	4,971.6	144,028.8	1,675.3	11,936.3	4.90	244.9
51	0.85	726.8	6,177.4	5,260.1	157,523.1	1,726.0	12,298.0	5.05	252.3
52-1/2	0.85	748.1	6,546.1	5,556.1	171,835.0	1,776.8	12,659.7	5.20	259.8
54	0.85	769.5	6,925.5	5,859.8	186,988.5	1,827.6	13,021.4	5.34	267.2
55-1/2	0.84	790.9	7,315.6	6,171.0	203,007.7	1,878.3	13,383.1	5.49	274.6
57	0.84	812.3	7,716.4	6,489.8	219,916.7	1,929.1	13,744.8	5.64	282.0
58-1/2	0.84	833.6	8,127.8	6,816.2	237,739.4	1,979.9	14,106.5	5.79	289.5
60	0.84	855.0	8,550.0	7,150.1	256,500.0	2,030.6	14,468.2	5.94	296.9
61-1/2	0.83	876.4	8,982.8	7,491.5	276,222.4	2,081.4	14,829.9	6.09	304.3
63	0.83	897.8	9,426.4	7,840.3	296,930.8	2,132.2	15,191.6	6.23	311.7
64-1/2	0.83	919.1	9,880.6	8,196.7	318,649.1	2,182.9	15,553.3	6.38	319.1
66	0.83	940.5	10,345.5	8,560.5	341,401.5	2,233.7	15,915.0	6.53	326.6
67-1/2	0.83	961.9	10,821.1	8,931.7	365,211.9	2,284.5	16,276.7	6.68	334.0
69	0.82	983.3	11,307.4	9,310.3	390,104.4	2,335.2	16,638.4	6.83	341.4
70-1/2	0.82	1,004.6	11,804.3	9,696.3	416,103.1	2,386.0	17,000.1	6.98	348.8
72	0.82	1,026.0	12,312.0	10,089.6	443,232.0	2,436.8	17,361.8	7.13	356.3
73-1/2	0.82	1,047.4	12,830.3	10,490.4	471,515.1	2,487.5	17,723.5	7.27	363.7
75	0.82	1,068.8	13,359.4	10,898.4	500,976.6	2,538.3	18,085.3	7.42	371.1
76-1/2	0.81	1,090.1	13,899.1	11,313.8	531,640.3	2,589.0	18,447.0	7.57	378.5
78	0.81	1,111.5	14,449.5	11,736.5	563,530.5	2,639.8	18,808.7	7.72	385.9

<sup>a</sup>Based on a unit weight of 50 lb/ft<sup>3</sup>.

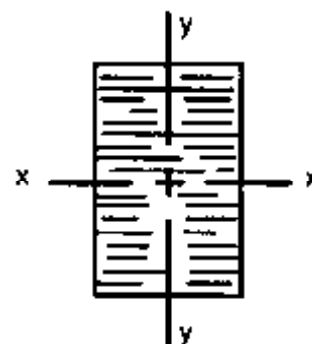


Table 16-3. - Section properties for structural glulam manufactured from western species with 1-1/2-inch-thick laminations *(continued)*.

Depth <i>d</i> (in.)	Size factor <i>C<sub>F</sub></i>	Area <i>A</i> (in <sup>2</sup> )	X-X axis			Y-Y axis		Volume (ft <sup>3</sup> /ft)	Weight <sup>a</sup> (lb/ft)
			<i>S<sub>x</sub></i> (in <sup>3</sup> )	<i>S<sub>x</sub>C<sub>F</sub></i> (in <sup>3</sup> )	<i>I<sub>x</sub></i> (in <sup>4</sup> )	<i>S<sub>y</sub></i> (in <sup>3</sup> )	<i>I<sub>y</sub></i> (in <sup>4</sup> )		
14-1/4-inch width (continued)									
79-1/2	0.81	1,132.9	15,010.6	12,166.5	596,671.1	2,690.6	19,170.4	7.87	393.4
81	0.81	1,154.3	15,582.4	12,603.7	631,086.2	2,741.3	19,532.1	8.02	400.8
82-1/2	0.81	1,175.6	16,164.8	13,048.2	666,799.8	2,792.1	19,893.8	8.16	408.2
84	0.81	1,197.0	16,758.0	13,499.9	703,836.0	2,842.9	20,255.5	8.31	415.6
85-1/2	0.80	1,218.4	17,361.8	13,958.9	742,218.8	2,893.6	20,617.2	8.46	423.0
87	0.80	1,239.8	17,976.4	14,425.1	781,972.3	2,944.4	20,978.9	8.61	430.5
88-1/2	0.80	1,261.1	18,601.6	14,898.5	823,120.5	2,995.2	21,340.6	8.76	437.9
90	0.80	1,282.5	19,237.5	15,379.0	865,687.5	3,045.9	21,702.3	8.91	445.3
91-1/2	0.80	1,303.9	19,884.1	15,866.8	909,697.3	3,096.7	22,064.0	9.05	452.7
93	0.80	1,325.3	20,541.4	16,361.7	955,173.9	3,147.5	22,425.7	9.20	460.2
94-1/2	0.80	1,346.6	21,209.3	16,863.7	1,002,141.5	3,198.2	22,787.4	9.35	467.6
96	0.79	1,368.0	21,888.0	17,372.9	1,050,624.0	3,249.0	23,149.1	9.50	475.0

<sup>a</sup> Based on a unit weight of 50 lb/ft<sup>3</sup>.

Table 16-4 - Section properties for structural glulam manufactured from Southern Pine with 1-3/8-inch-thick laminations.



Depth <i>d</i> (in.)	Size factor <i>C<sub>F</sub></i>	Area <i>A</i> (in <sup>2</sup> )	X-X axis			Y-Y axis		Volume (ft <sup>3</sup> /ft)	Weight <sup>a</sup> (lb/ft)
			<i>S<sub>x</sub></i> (in <sup>3</sup> )	<i>S<sub>x</sub>C<sub>F</sub></i> (in <sup>3</sup> )	<i>I<sub>x</sub></i> (in <sup>4</sup> )	<i>S<sub>y</sub></i> (in <sup>3</sup> )	<i>I<sub>y</sub></i> (in <sup>4</sup> )		
3-inch width									
2-3/4	1.00	8.3	3.8	3.8	5.2	4.1	6.2	0.06	2.9
4-1/8	1.00	12.4	8.5	8.5	17.5	6.2	9.3	0.09	4.3
5-1/2	1.00	16.5	15.1	15.1	41.6	8.3	12.4	0.11	5.7
6-7/8	1.00	20.6	23.6	23.6	81.2	10.3	15.5	0.14	7.2
8-1/4	1.00	24.8	34.0	34.0	140.4	12.4	18.6	0.17	8.6
9-5/8	1.00	28.9	46.3	46.3	222.9	14.4	21.7	0.20	10.0
11	1.00	33.0	60.5	60.5	332.8	16.5	24.8	0.23	11.5
12-3/8	1.00	37.1	76.6	76.3	473.8	18.6	27.8	0.26	12.9
13-3/4	0.98	41.3	94.5	93.1	649.9	20.6	30.9	0.29	14.3
15-1/8	0.97	45.4	114.4	111.5	865.0	22.7	34.0	0.32	15.8
16-1/2	0.97	49.5	136.1	131.4	1,123.0	24.8	37.1	0.34	17.2
17-7/8	0.96	53.6	159.8	152.8	1,427.8	26.8	40.2	0.37	18.6
19-1/4	0.95	57.8	185.3	175.8	1,783.3	28.9	43.3	0.40	20.1
20-5/8	0.94	61.9	212.7	200.3	2,193.4	30.9	46.4	0.43	21.5
22	0.93	66.0	242.0	226.2	2,662.0	33.0	49.5	0.46	22.9
23-3/8	0.93	70.1	273.2	253.7	3,193.0	35.1	52.6	0.49	24.3
24-3/4	0.92	74.3	306.3	282.6	3,790.2	37.1	55.7	0.52	25.8
26-1/8	0.92	78.4	341.3	313.0	4,457.7	39.2	58.8	0.54	27.2
27-1/2	0.91	82.5	378.1	344.8	5,199.2	41.3	61.9	0.57	28.6
28-7/8	0.91	86.6	416.9	378.1	6,018.7	43.3	65.0	0.60	30.1
30-1/4	0.90	90.8	457.5	412.9	6,920.2	45.4	68.1	0.63	31.5
5-inch width									
2-3/4	1.00	13.8	6.3	6.3	8.7	11.5	28.6	0.10	4.8
4-1/8	1.00	20.6	14.2	14.2	29.2	17.2	43.0	0.14	7.2
5-1/2	1.00	27.5	25.2	25.2	69.3	22.9	57.3	0.19	9.5
6-7/8	1.00	34.4	39.4	39.4	135.4	28.6	71.6	0.24	11.9
8-1/4	1.00	41.3	56.7	56.7	234.0	34.4	85.9	0.29	14.3
9-5/8	1.00	48.1	77.2	77.2	371.5	40.1	100.3	0.33	16.7
11	1.00	55.0	100.8	100.8	554.6	45.8	114.6	0.38	19.1

<sup>a</sup>Based on a unit weight of 50 lb/ft<sup>3</sup>.

Table 16-4. - Section properties for structural glulam manufactured from Southern Pine with 1-3/8-inch-thick laminations (*continued*).

Depth <i>d</i> (In.)	Size factor <i>C<sub>F</sub></i>	Area <i>A</i> (In <sup>2</sup> )	X-X axis			Y-Y axis		Volume (ft <sup>3</sup> /ft)	Weight <sup>a</sup> (lb/ft)
			<i>S<sub>x</sub></i> (In <sup>3</sup> )	<i>S<sub>x</sub>C<sub>F</sub></i> (In <sup>3</sup> )	<i>I<sub>x</sub></i> (In <sup>4</sup> )	<i>S<sub>y</sub></i> (In <sup>3</sup> )	<i>I<sub>y</sub></i> (In <sup>4</sup> )		
5-inch width (continued)									
12-3/8	1.00	61.9	127.6	127.2	789.6	51.6	128.9	0.43	21.5
13-3/4	0.98	68.8	157.6	155.2	1,083.2	57.3	143.2	0.48	23.9
15-1/8	0.97	75.6	190.6	185.8	1,441.7	63.0	157.6	0.53	26.3
16-1/2	0.97	82.5	226.9	219.0	1,871.7	68.8	171.9	0.57	28.6
17-7/8	0.96	89.4	266.3	254.7	2,379.7	74.5	186.2	0.62	31.0
19-1/4	0.95	96.3	308.8	293.0	2,972.2	80.2	200.5	0.67	33.4
20-5/8	0.94	103.1	354.5	333.8	3,655.7	85.9	214.8	0.72	35.8
22	0.93	110.0	403.3	377.1	4,436.7	91.7	229.2	0.76	38.2
23-3/8	0.93	116.9	455.3	422.8	5,321.6	97.4	243.5	0.81	40.6
24-3/4	0.92	123.8	510.5	471.0	6,317.1	103.1	257.8	0.86	43.0
26-1/8	0.92	130.6	568.8	521.7	7,429.5	108.9	272.1	0.91	45.4
27-1/2	0.91	137.5	630.2	574.7	8,665.4	114.6	286.5	0.95	47.7
28-7/8	0.91	144.4	694.8	630.2	10,031.2	120.3	300.8	1.00	50.1
30-1/4	0.90	151.3	762.6	688.1	11,533.6	126.0	315.1	1.05	52.5
31-5/8	0.90	158.1	833.5	748.4	13,178.9	131.8	329.4	1.10	54.9
33	0.89	165.0	907.5	811.0	14,973.8	137.5	343.8	1.15	57.3
34-3/8	0.89	171.9	984.7	876.0	16,924.5	143.2	358.1	1.19	59.7
35-3/4	0.89	178.8	1,065.1	943.4	19,037.8	149.0	372.4	1.24	62.1
6-3/4-inch width									
5-1/2	1.00	37.1	34.0	34.0	93.6	41.8	141.0	0.26	12.9
6-7/8	1.00	46.4	53.2	53.2	182.8	52.2	176.2	0.32	16.1
8-1/4	1.00	55.7	76.6	76.6	315.9	62.6	211.4	0.39	19.3
9-5/8	1.00	65.0	104.2	104.2	501.6	73.1	246.7	0.45	22.6
11	1.00	74.3	136.1	136.1	748.7	83.5	281.9	0.52	25.8
12-3/8	1.00	83.5	172.3	171.7	1,066.0	94.0	317.2	0.58	29.0
13-3/4	0.98	92.8	212.7	209.5	1,462.3	104.4	352.4	0.64	32.2
15-1/8	0.97	102.1	257.4	250.8	1,946.3	114.9	387.6	0.71	35.4
16-1/2	0.97	111.4	306.3	295.6	2,526.8	125.3	422.9	0.77	38.7
17-7/8	0.96	120.7	359.5	343.9	3,212.6	135.7	458.1	0.84	41.9
19-1/4	0.95	129.9	416.9	395.6	4,012.5	146.2	493.4	0.90	45.1
20-5/8	0.94	139.2	478.6	450.6	4,935.2	156.6	528.6	0.97	48.3
22	0.93	148.5	544.5	509.0	5,989.5	167.1	563.8	1.03	51.6
23-3/8	0.93	157.8	614.7	570.8	7,184.2	177.5	599.1	1.10	54.8
24-3/4	0.92	167.1	689.1	635.9	8,528.0	187.9	634.3	1.16	58.0
26-1/8	0.92	176.3	767.8	704.2	10,029.8	198.4	669.6	1.22	61.2
27-1/2	0.91	185.6	850.8	775.9	11,698.2	208.8	704.8	1.29	64.5
28-7/8	0.91	194.9	938.0	850.8	13,542.2	219.3	740.0	1.35	67.7
30-1/4	0.90	204.2	1,029.4	928.9	15,570.4	229.7	775.3	1.42	70.9
31-5/8	0.90	213.5	1,125.2	1,010.3	17,791.6	240.2	810.5	1.48	74.1
33	0.89	222.8	1,225.1	1,094.9	20,214.6	250.6	845.8	1.55	77.3
34-3/8	0.89	232.0	1,329.3	1,182.6	22,848.1	261.0	881.0	1.61	80.6
35-3/4	0.89	241.3	1,437.8	1,273.6	25,701.0	271.5	916.2	1.68	83.8
37-1/8	0.88	250.6	1,550.5	1,367.7	28,782.1	281.9	951.5	1.74	87.0
38-1/2	0.88	259.9	1,667.5	1,464.9	32,100.0	292.4	986.7	1.80	90.2

<sup>a</sup>Based on a unit weight of 50 lb/ft<sup>3</sup>.

Table 16-4. - Section properties for structural glulam manufactured from Southern Pine with 1-3/8-inch-thick laminations (*continued*).

Depth <i>d</i> (in.)	Size factor <i>C<sub>F</sub></i>	Area <i>A</i> (in <sup>2</sup> )	X-X axis			Y-Y axis		Volume (ft <sup>3</sup> /ft)	Weight <sup>a</sup> (lb/ft)
			<i>S<sub>x</sub></i> (in <sup>3</sup> )	<i>S<sub>x</sub>C<sub>F</sub></i> (in <sup>3</sup> )	<i>I<sub>x</sub></i> (in <sup>4</sup> )	<i>S<sub>y</sub></i> (in <sup>3</sup> )	<i>I<sub>y</sub></i> (in <sup>4</sup> )		
6-3/4-inch width (continued)									
39-7/8	0.88	269.2	1,788.8	1,565.3	35,663.6	302.8	1,022.0	1.87	93.5
41-1/4	0.87	278.4	1,914.3	1,668.9	39,481.6	313.2	1,057.2	1.93	96.7
42-5/8	0.87	287.7	2,044.0	1,775.5	43,562.8	323.7	1,092.4	2.00	99.9
44	0.87	297.0	2,178.0	1,885.2	47,916.0	334.1	1,127.7	2.06	103.1
45-3/8	0.86	306.3	2,316.3	1,998.0	52,550.0	344.6	1,162.9	2.13	106.3
46-3/4	0.86	315.6	2,458.8	2,113.9	57,473.5	355.0	1,198.2	2.19	109.6
48-1/8	0.86	324.8	2,605.5	2,232.9	62,695.3	365.4	1,233.4	2.26	112.8
8-1/2-inch width									
8-1/4	1.00	70.1	96.4	96.4	397.7	99.3	422.2	0.49	24.3
9-5/8	1.00	81.8	131.2	131.2	631.6	115.9	492.6	0.57	28.4
11	1.00	93.5	171.4	171.4	942.8	132.5	562.9	0.65	32.5
12-3/8	1.00	105.2	216.9	216.2	1,342.4	149.0	633.3	0.73	36.5
13-3/4	0.98	116.9	267.8	263.8	1,841.4	165.6	703.7	0.81	40.6
15-1/8	0.97	128.6	324.1	315.9	2,450.9	182.1	774.1	0.89	44.6
16-1/2	0.97	140.3	385.7	372.3	3,181.9	198.7	844.4	0.97	48.7
17-7/8	0.96	151.9	452.6	433.0	4,045.5	215.2	914.8	1.06	52.8
19-1/4	0.95	163.6	525.0	498.1	5,052.8	231.8	985.2	1.14	56.8
20-5/8	0.94	175.3	602.6	567.4	6,214.7	248.4	1,055.5	1.22	60.9
22	0.93	187.0	685.7	641.0	7,542.3	264.9	1,125.9	1.30	64.9
23-3/8	0.93	198.7	774.1	718.8	9,046.7	281.5	1,196.3	1.38	69.0
24-3/4	0.92	210.4	867.8	800.7	10,739.0	298.0	1,266.6	1.46	73.0
26-1/8	0.92	222.1	966.9	886.8	12,630.1	314.6	1,337.0	1.54	77.1
27-1/2	0.91	233.8	1,071.4	977.0	14,731.1	331.1	1,407.4	1.62	81.2
28-7/8	0.91	245.4	1,181.2	1,071.4	17,053.1	347.7	1,477.7	1.70	85.2
30-1/4	0.90	257.1	1,296.3	1,169.8	19,607.1	364.3	1,548.1	1.79	89.3
31-5/8	0.90	268.8	1,416.9	1,272.2	22,404.2	380.8	1,618.5	1.87	93.3
33	0.89	280.5	1,542.8	1,378.7	25,455.4	397.4	1,688.8	1.95	97.4
34-3/8	0.89	292.2	1,674.0	1,489.3	28,771.7	413.9	1,759.2	2.03	101.5
35-3/4	0.89	303.9	1,810.6	1,603.8	32,364.3	430.5	1,829.6	2.11	105.5
37-1/8	0.88	315.6	1,952.5	1,722.3	36,244.1	447.0	1,899.9	2.19	109.6
38-1/2	0.88	327.3	2,099.9	1,844.7	40,422.2	463.6	1,970.3	2.27	113.6
39-7/8	0.88	338.9	2,252.5	1,971.2	44,909.7	480.2	2,040.7	2.35	117.7
41-1/4	0.87	350.6	2,410.5	2,101.5	49,717.5	496.7	2,111.1	2.43	121.7
42-5/8	0.87	362.3	2,573.9	2,235.8	54,856.8	513.3	2,181.4	2.52	125.8
44	0.87	374.0	2,742.7	2,374.0	60,338.7	529.8	2,251.8	2.60	129.9
45-3/8	0.86	385.7	2,916.8	2,516.0	66,174.0	546.4	2,322.2	2.68	133.9
46-3/4	0.86	397.4	3,096.2	2,662.0	72,374.0	562.9	2,392.5	2.76	138.0
48-1/8	0.86	409.1	3,281.0	2,811.8	78,949.6	579.5	2,462.9	2.84	142.0
49-1/2	0.85	420.8	3,471.2	2,965.5	85,911.9	596.1	2,533.3	2.92	146.1
50-7/8	0.85	432.4	3,666.7	3,123.0	93,271.9	612.6	2,603.6	3.00	150.2
52-1/4	0.85	444.1	3,867.6	3,284.4	101,040.8	629.2	2,674.0	3.08	154.2
53-5/8	0.85	455.8	4,073.8	3,449.5	109,229.4	645.7	2,744.4	3.17	158.3
55	0.84	467.5	4,285.4	3,618.5	117,849.0	662.3	2,814.7	3.25	162.3
56-3/8	0.84	479.2	4,502.4	3,791.3	126,910.4	678.8	2,885.1	3.33	166.4

<sup>a</sup>Based on a unit weight of 50 lb/ft<sup>3</sup>.

Table 16-4. - Section properties for structural glulam manufactured from Southern Pine with 1-3/8-inch-thick laminations (*continued*).

Depth <i>d</i> (in.)	Size factor <i>C<sub>F</sub></i>	Area <i>A</i> (in <sup>2</sup> )	X-X axis			Y-Y axis		Volume (ft <sup>3</sup> /ft)	Weight <sup>a</sup> (lb/ft)
			<i>S<sub>x</sub></i> (in <sup>3</sup> )	<i>S<sub>x</sub>C<sub>F</sub></i> (in <sup>3</sup> )	<i>I<sub>x</sub></i> (in <sup>4</sup> )	<i>S<sub>y</sub></i> (in <sup>3</sup> )	<i>I<sub>y</sub></i> (in <sup>4</sup> )		
8-1/2-inch width (continued)									
57-3/4	0.84	490.9	4,724.7	3,967.8	136,424.9	695.4	2,955.5	3.41	170.4
59-1/8	0.84	502.6	4,952.3	4,148.2	146,403.4	712.0	3,025.8	3.49	174.5
60-1/2	0.84	514.3	5,185.4	4,332.3	156,857.0	728.5	3,096.2	3.57	178.6
61-7/8	0.83	525.9	5,423.7	4,520.1	167,796.7	745.1	3,166.6	3.65	182.6
10-1/2-inch width									
11	1.00	115.5	211.8	211.8	1,164.6	202.1	1,061.2	0.80	40.1
12-3/8	1.00	129.9	268.0	267.1	1,658.2	227.4	1,193.8	0.90	45.1
13-3/4	0.98	144.4	330.9	325.9	2,274.7	252.7	1,326.4	1.00	50.1
15-1/8	0.97	158.8	400.3	390.2	3,027.6	277.9	1,459.1	1.10	55.1
16-1/2	0.97	173.3	476.4	459.9	3,930.6	303.2	1,591.7	1.20	60.2
17-7/8	0.96	187.7	559.2	534.9	4,997.4	328.5	1,724.4	1.30	65.2
19-1/4	0.95	202.1	648.5	615.3	6,241.7	353.7	1,857.0	1.40	70.2
20-5/8	0.94	216.6	744.4	701.0	7,677.0	379.0	1,989.7	1.50	75.2
22	0.93	231.0	847.0	791.8	9,317.0	404.3	2,122.3	1.60	80.2
23-3/8	0.93	245.4	956.2	887.9	11,175.4	429.5	2,255.0	1.70	85.2
24-3/4	0.92	259.9	1,072.0	989.1	13,265.8	454.8	2,387.6	1.80	90.2
26-1/8	0.92	274.3	1,194.4	1,095.5	15,601.9	480.0	2,520.2	1.90	95.2
27-1/2	0.91	288.8	1,323.4	1,206.9	18,197.3	505.3	2,652.9	2.01	100.3
28-7/8	0.91	303.2	1,459.1	1,323.5	21,065.6	530.6	2,785.5	2.11	105.3
30-1/4	0.90	317.6	1,601.4	1,445.0	24,220.6	555.8	2,918.2	2.21	110.3
31-5/8	0.90	332.1	1,750.2	1,571.6	27,675.8	581.1	3,050.8	2.31	115.3
33	0.89	346.5	1,905.8	1,703.1	31,444.9	606.4	3,183.5	2.41	120.3
34-3/8	0.89	360.9	2,067.9	1,839.7	35,541.5	631.6	3,316.1	2.51	125.3
35-3/4	0.89	375.4	2,236.6	1,981.1	39,979.4	656.9	3,448.8	2.61	130.3
37-1/8	0.88	389.8	2,412.0	2,127.5	44,772.1	682.2	3,581.4	2.71	135.4
38-1/2	0.88	404.3	2,593.9	2,278.8	49,933.3	707.4	3,714.0	2.81	140.4
39-7/8	0.88	418.7	2,782.5	2,435.0	55,476.6	732.7	3,846.7	2.91	145.4
41-1/4	0.87	433.1	2,977.7	2,596.0	61,415.8	758.0	3,979.3	3.01	150.4
42-5/8	0.87	447.6	3,179.6	2,761.9	67,764.3	783.2	4,112.0	3.11	155.4
44	0.87	462.0	3,388.0	2,932.6	74,536.0	808.5	4,244.6	3.21	160.4
45-3/8	0.86	476.4	3,603.1	3,108.1	81,744.4	833.8	4,377.3	3.31	165.4
46-3/4	0.86	490.9	3,824.7	3,288.4	89,403.2	859.0	4,509.9	3.41	170.4
48-1/8	0.86	505.3	4,053.0	3,473.4	97,526.0	884.3	4,642.6	3.51	175.5
49-1/2	0.85	519.8	4,287.9	3,663.3	106,126.5	909.6	4,775.2	3.61	180.5
50-7/8	0.85	534.2	4,529.5	3,857.8	115,218.3	934.8	4,907.8	3.71	185.5
52-1/4	0.85	548.6	4,777.6	4,057.2	124,815.0	960.1	5,040.5	3.81	190.5
53-5/8	0.85	563.1	5,032.4	4,261.2	134,930.4	985.4	5,173.1	3.91	195.5
55	0.84	577.5	5,293.8	4,469.9	145,578.1	1,010.6	5,305.8	4.01	200.5
56-3/8	0.84	591.9	5,561.7	4,683.3	156,771.7	1,035.9	5,438.4	4.11	205.5
57-3/4	0.84	606.4	5,836.4	4,901.4	168,524.9	1,061.2	5,571.1	4.21	210.5
59-1/8	0.84	620.8	6,117.6	5,124.2	180,851.2	1,086.4	5,703.7	4.31	215.6
60-1/2	0.84	635.3	6,405.4	5,351.6	193,764.5	1,111.7	5,836.4	4.41	220.6
61-7/8	0.83	649.7	6,699.9	5,583.7	207,278.2	1,137.0	5,969.0	4.51	225.6
63-1/4	0.83	664.1	7,001.0	5,820.4	221,406.1	1,162.2	6,101.6	4.61	230.6

<sup>a</sup>Based on a unit weight of 50 lb/ft<sup>3</sup>.

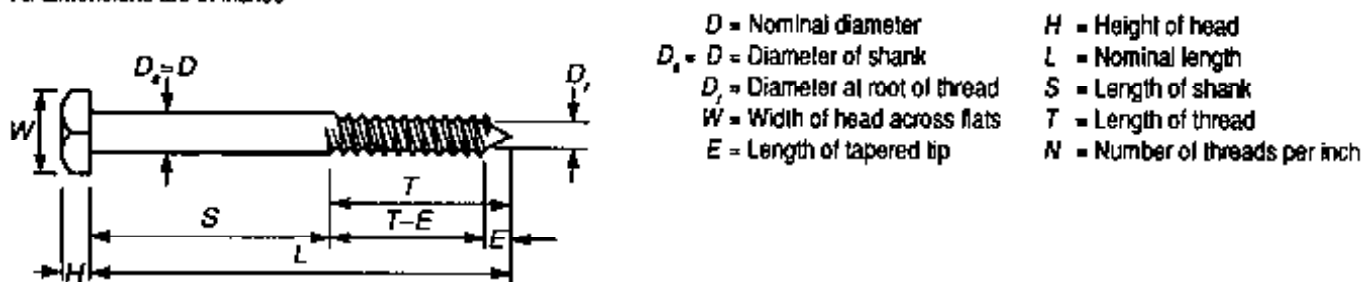
Table 16-4. - Section properties for structural glulam manufactured from Southern Pine with 1-3/8-inch-thick laminations *(continued)*.

Depth <i>d</i> (in.)	Size factor <i>C<sub>F</sub></i>	Area <i>A</i> (in <sup>2</sup> )	X-X axis			Y-Y axis		Volume (ft <sup>3</sup> /ft)	Weight <sup>a</sup> (lb/ft)
			<i>S<sub>x</sub></i> (in <sup>3</sup> )	<i>S<sub>x</sub>C<sub>F</sub></i> (in <sup>3</sup> )	<i>I<sub>x</sub></i> (in <sup>4</sup> )	<i>S<sub>y</sub></i> (in <sup>3</sup> )	<i>I<sub>y</sub></i> (in <sup>4</sup> )		
10-1/2-inch width (continued)									
64-5/8	0.83	678.6	7,308.7	6,061.7	236,161.8	1,187.5	6,234.3	4.71	235.6
66	0.83	693.0	7,623.0	6,307.6	251,559.0	1,212.8	6,366.9	4.81	240.6
67-3/8	0.83	707.4	7,943.9	6,558.1	267,611.3	1,238.0	6,499.6	4.91	245.6
68-3/4	0.82	721.9	8,271.5	6,813.2	284,332.3	1,263.3	6,632.2	5.01	250.7
70-1/8	0.82	736.3	8,605.7	7,072.9	301,735.7	1,288.5	6,764.9	5.11	255.7
71-1/2	0.82	750.8	8,946.4	7,337.1	319,835.1	1,313.8	6,897.5	5.21	260.7
72-7/8	0.82	765.2	9,293.8	7,605.9	338,644.3	1,339.1	7,030.2	5.31	265.7
74-1/4	0.82	779.6	9,647.9	7,879.2	358,176.8	1,364.3	7,162.8	5.41	270.7
75-5/8	0.82	794.1	10,008.5	8,157.1	378,446.3	1,389.6	7,295.4	5.51	275.7

<sup>a</sup> Based on a unit weight of 50 lb/ft<sup>3</sup>.

Table 16-5. - Typical dimensions of standard lag screws for wood.

All dimensions are in inches



Nominal length, L (in.) <sup>a</sup>	Item	Dimension of lag screws with various nominal diameters D									
		1/4	3/8	1/2	9/16	5/8	3/4	7/8	1	1-1/8	1-1/4
All lengths	$D_s = D$	0.250	0.375	0.500	0.5625	0.625	0.750	0.875	1.000	1.125	1.250
	$D_r$	0.173	0.265	0.371	0.435	0.471	0.579	0.683	0.780	0.887	1.012
	E	3/16	1/4	5/16	3/8	3/8	7/16	1/2	9/16	5/8	3/4
	H	11/64	1/4	21/64	3/8	27/64	1/2	19/32	21/32	3/4	27/32
	W	3/8	9/16	3/4	7/8	15/16	1-1/8	1-5/16	1-1/2	1-11/16	1-7/8
	N	10	7	6	6	5	4-1/2	4	3-1/2	3-1/4	3-1/4
4	S	1-1/2	1-1/2	1-1/2	1-1/2	1-1/2	1-1/2	1-1/2	1-1/2	1-1/2	1-1/2
	T	2-1/2	2-1/2	2-1/2	2-1/2	2-1/2	2-1/2	2-1/2	2-1/2	2-1/2	2-1/2
	T-E	2-5/16	2-1/4	2-3/16	2-1/8	2-1/8	2-1/16	2	1-15/16	1-7/8	1-3/4
5	S	2	2	2	2	2	2	2	2	2	2
	T	3	3	3	3	3	3	3	3	3	3
	T-E	2-13/16	2-3/4	2-11/16	2-5/8	2-5/8	2-9/16	2-1/2	2-7/16	2-3/8	2-1/4
6	S	2-1/2	2-1/2	2-1/2	2-1/2	2-1/2	2-1/2	2-1/2	2-1/2	2-1/2	2-1/2
	T	3-1/2	3-1/2	3-1/2	3-1/2	3-1/2	3-1/2	3-1/2	3-1/2	3-1/2	3-1/2
	T-E	3-5/16	3-1/4	3-3/16	3-1/8	3-1/8	3-1/16	3	2-15/16	2-7/8	2-3/4
7	S	3	3	3	3	3	3	3	3	3	3
	T	4	4	4	4	4	4	4	4	4	4
	T-E	3-13/16	3-3/4	3-11/16	3-5/8	3-5/8	3-9/16	3-1/2	3-7/16	3-3/8	3-1/4
8	S	3-1/2	3-1/2	3-1/2	3-1/2	3-1/2	3-1/2	3-1/2	3-1/2	3-1/2	3-1/2
	T	4-1/2	4-1/2	4-1/2	4-1/2	4-1/2	4-1/2	4-1/2	4-1/2	4-1/2	4-1/2
	T-E	4-5/16	4-1/4	4-3/16	4-1/8	4-1/8	4-1/16	4	3-15/16	3-7/8	3-3/4
9	S	4	4	4	4	4	4	4	4	4	4
	T	5	5	5	5	5	5	5	5	5	5
	T-E	4-13/16	4-3/4	4-11/16	4-5/8	4-5/8	4-9/16	4-1/2	4-7/16	4-3/8	4-1/4
10	S	4-3/4	4-3/4	4-3/4	4-3/4	4-3/4	4-3/4	4-3/4	4-3/4	4-3/4	4-3/4
	T	5-1/4	5-1/4	5-1/4	5-1/4	5-1/4	5-1/4	5-1/4	5-1/4	5-1/4	5-1/4
	T-E	5-1/16	5	4-15/16	4-7/8	4-7/8	4-13/16	4-3/4	4-11/16	4-5/8	4-1/2
11	S	5-1/2	5-1/2	5-1/2	5-1/2	5-1/2	5-1/2	5-1/2	5-1/2	5-1/2	5-1/2
	T	5-1/2	5-1/2	5-1/2	5-1/2	5-1/2	5-1/2	5-1/2	5-1/2	5-1/2	5-1/2
	T-E	5-9/32	5-1/4	5-3/16	5-1/8	5-1/8	5-1/16	5	4-15/16	4-7/8	4-3/4
12	S	6	6	6	6	6	6	6	6	6	6
	T	6	6	6	6	6	6	6	6	6	6
	T-E	5-13/16	5-3/4	5-11/16	5-5/8	5-5/8	5-9/16	5-1/2	5-7/16	5-3/8	5-1/4

<sup>a</sup>Length of thread T on intervening bolt lengths is the same as that of the next shorter length listed. The length of thread T on standard lag screw lengths in excess of 12 inches is equal to one-half the lag screw length, L/2.

Table 16-6. - Typical dimensions for timber connectors.

Split rings	Dimensions (in.)	
	2-1/2 in.	4 in.
Split ring		
Inside diameter at center when closed	2.500	4.000
Thickness of metal at center	0.163	0.193
Depth of metal (width of ring) 0.750	1.000	
Groove		
Inside diameter	2.56	4.08
Width	0.18	0.21
Depth	0.375	0.50
Bolt hole, diameter in timber	9/16	13/16
Washers, standard		
Round, cast or malleable iron, diameter	2-5/8	3
Round, wrought iron (minimum)		
Diameter	1-3/8	2
Thickness	3/32	5/32
Square plate		
Length of side	2	3
Thickness	1/8	3/16
Projected area		
Portion of one ring within member (in <sup>2</sup> )	1.10	2.24



**Table 16-6. - Typical dimensions for timber connectors (continued).**

Shear plates	Dimensions (in.)			
	2-5/8 in.	2-5/8 in.	4-in.	4-in.
Shear plate, material	Pressed steel	Light gage	Malleable iron	Malleable iron
Diameter of plate	2.62	2.62	4.03	4.03
Diameter of hole	0.81	0.81	0.81	0.94
Thickness of plate	0.17	0.12	0.20	0.20
Depth of plate	0.42	0.35	0.64	0.64
Dolt hole, diameter in timber	13/16	13/16	13/16	15/16
Washers, standard				
Round, cast or malleable iron, diameter	3	3	3	3-1/2
Round, wrought iron, minimum				
Diameter	2	2	2	2-1/4
Thickness	5/32	5/32	5/32	11/64
Square Plate				
Length of side	3	3	3	3
Thickness	1/4	1/4	1/4	1/4
Projected area				
Portion of one shear plate within member (in <sup>2</sup> )	1.18	1.00	2.58	2.58

Table 16-7. - Typical dimensions and weights for malleable iron washers.



Bolt size (in.)	Outside diameter (in.)	Inside diameter (in.)	Thickness (in.)	Weight per 100 pieces (lb)	Number in 100 lb
3/8	2-1/2	5/8	1/4	20	500
1/2	2-1/2	5/8	1/4	23	435
5/8	2-3/4	3/4	5/16	26	385
3/4	3	7/8	7/16	40	250
7/8	3-1/2	1	7/16	54	185
1	4	1-1/8	1/2	72	139
1-1/8	4-1/2	1-1/4	1/2	108	93
1-1/4	5	1-3/8	9/16	144	69
1-3/8	5-1/2	1-1/2	5/8	150	67
1-1/2	6	1-5/8	3/4	182	55
1-3/4	6	1-7/8	3/4	255	39
2	7-1/2	2-1/8	3/4	420	24

Table 16-8. - Maximum vehicle moment, reaction, and deflection coefficient.  
Simple span, one wheel line, impact factor not included.

Vehicle type H 15-44

Span (ft)	Moment <sup>a</sup> (ft-kips)	Reaction <sup>a</sup> (kips)	Deflection <sup>b</sup> coefficient	Span (ft)	Moment (ft-kips)	Reaction <sup>a</sup> (kips)	Deflection <sup>b</sup> coefficient	Span (ft)	Moment (ft-kips)	Reaction <sup>a</sup> (kips)	Deflection <sup>b</sup> coefficient
10	30.00	12.00	$4.32 \times 10^8$	47	155.88	15.39 <sup>c</sup>	$5.19 \times 10^{10}$	84	353.43 <sup>c</sup>	19.83 <sup>c</sup>	$4.13 \times 10^{11c}$
11	33.00	12.00	$5.75 \times 10^8$	48	159.61	15.51 <sup>c</sup>	$5.55 \times 10^{10}$	85	360.19 <sup>c</sup>	19.95 <sup>c</sup>	$4.31 \times 10^{11c}$
12	36.00	12.00	$7.46 \times 10^8$	49	163.35	15.63 <sup>c</sup>	$5.92 \times 10^{10}$	86	367.01 <sup>c</sup>	20.07 <sup>c</sup>	$4.50 \times 10^{11c}$
13	39.00	12.00	$9.49 \times 10^8$	50	167.09	15.75 <sup>c</sup>	$6.31 \times 10^{10}$	87	373.88 <sup>c</sup>	20.19 <sup>c</sup>	$4.69 \times 10^{11c}$
14	42.00	12.00	$1.19 \times 10^9$	51	170.83	15.87 <sup>c</sup>	$6.71 \times 10^{10}$	88	380.82 <sup>c</sup>	20.31 <sup>c</sup>	$4.89 \times 10^{11c}$
15	45.00	12.20	$1.48 \times 10^9$	52	174.57	15.99 <sup>c</sup>	$7.13 \times 10^{10}$	89	387.82 <sup>c</sup>	20.43 <sup>c</sup>	$5.10 \times 10^{11c}$
16	48.00	12.38	$1.77 \times 10^9$	53	178.30	16.11 <sup>c</sup>	$7.57 \times 10^{10}$	90	394.88 <sup>c</sup>	20.55 <sup>c</sup>	$5.31 \times 10^{11c}$
17	51.00	12.53	$2.12 \times 10^9$	54	182.04	16.23 <sup>c</sup>	$8.02 \times 10^{10}$	91	401.99 <sup>c</sup>	20.67 <sup>c</sup>	$5.53 \times 10^{11c}$
18	54.00	12.67	$2.52 \times 10^9$	55	185.78	16.35 <sup>c</sup>	$8.49 \times 10^{10}$	92	409.17 <sup>c</sup>	20.79 <sup>c</sup>	$5.76 \times 10^{11c}$
19	57.00	12.79	$2.96 \times 10^9$	56	189.53	16.47 <sup>c</sup>	$8.98 \times 10^{10}$	93	416.41 <sup>c</sup>	20.91 <sup>c</sup>	$5.99 \times 10^{11c}$
20	60.00	12.90	$3.46 \times 10^9$	57	193.66 <sup>c</sup>	16.59 <sup>c</sup>	$1.02 \times 10^{11c}$	94	423.71 <sup>c</sup>	21.03 <sup>c</sup>	$6.23 \times 10^{11c}$
21	63.00	13.00	$4.00 \times 10^9$	58	198.80 <sup>c</sup>	16.71 <sup>c</sup>	$1.09 \times 10^{11c}$	95	431.06 <sup>c</sup>	21.15 <sup>c</sup>	$6.48 \times 10^{11c}$
22	66.00	13.09	$4.60 \times 10^9$	59	203.99 <sup>c</sup>	16.83 <sup>c</sup>	$1.15 \times 10^{11c}$	96	438.48 <sup>c</sup>	21.27 <sup>c</sup>	$6.74 \times 10^{11c}$
23	69.00	13.17	$5.26 \times 10^9$	60	209.25 <sup>c</sup>	16.95 <sup>c</sup>	$1.22 \times 10^{11c}$	97	445.96 <sup>c</sup>	21.39 <sup>c</sup>	$7.00 \times 10^{11c}$
24	72.00	13.25	$5.97 \times 10^9$	61	214.57 <sup>c</sup>	17.07 <sup>c</sup>	$1.30 \times 10^{11c}$	98	453.50 <sup>c</sup>	21.51 <sup>c</sup>	$7.27 \times 10^{11c}$
25	75.00	13.32	$6.75 \times 10^9$	62	219.95 <sup>c</sup>	17.19 <sup>c</sup>	$1.38 \times 10^{11c}$	99	461.09 <sup>c</sup>	21.63 <sup>c</sup>	$7.55 \times 10^{11c}$
26	78.00	13.38	$7.59 \times 10^9$	63	225.38 <sup>c</sup>	17.31 <sup>c</sup>	$1.46 \times 10^{11c}$	100	468.75 <sup>c</sup>	21.75 <sup>c</sup>	$7.83 \times 10^{11c}$
27	81.34	13.44	$8.53 \times 10^9$	64	230.88 <sup>c</sup>	17.43 <sup>c</sup>	$1.54 \times 10^{11c}$	101	476.47 <sup>c</sup>	21.87 <sup>c</sup>	$8.12 \times 10^{11c}$
28	85.05	13.50	$9.65 \times 10^9$	65	236.44 <sup>c</sup>	17.55 <sup>c</sup>	$1.63 \times 10^{11c}$	102	484.25 <sup>c</sup>	21.99 <sup>c</sup>	$8.42 \times 10^{11c}$
29	88.76	13.55	$1.09 \times 10^{10}$	66	242.06 <sup>c</sup>	17.67 <sup>c</sup>	$1.72 \times 10^{11c}$	103	492.08 <sup>c</sup>	22.11 <sup>c</sup>	$8.73 \times 10^{11c}$
30	92.48	13.60	$1.22 \times 10^{10}$	67	247.73 <sup>c</sup>	17.79 <sup>c</sup>	$1.82 \times 10^{11c}$	104	499.98 <sup>c</sup>	22.23 <sup>c</sup>	$9.05 \times 10^{11c}$
31	96.20	13.65	$1.36 \times 10^{10}$	68	253.47 <sup>c</sup>	17.91 <sup>c</sup>	$1.92 \times 10^{11c}$	105	507.94 <sup>c</sup>	22.35 <sup>c</sup>	$9.38 \times 10^{11c}$
32	99.92	13.69	$1.51 \times 10^{10}$	69	259.27 <sup>c</sup>	18.03 <sup>c</sup>	$2.02 \times 10^{11c}$	106	515.96 <sup>c</sup>	22.47 <sup>c</sup>	$9.71 \times 10^{11c}$
33	103.64	13.73	$1.67 \times 10^{10}$	70	265.13 <sup>c</sup>	18.15 <sup>c</sup>	$2.13 \times 10^{11c}$	107	524.03 <sup>c</sup>	22.59 <sup>c</sup>	$1.01 \times 10^{12c}$
34	107.36	13.83 <sup>c</sup>	$1.84 \times 10^{10}$	71	271.04 <sup>c</sup>	18.27 <sup>c</sup>	$2.24 \times 10^{11c}$	108	532.17 <sup>c</sup>	22.71 <sup>c</sup>	$1.04 \times 10^{12c}$
35	111.09	13.95 <sup>c</sup>	$2.02 \times 10^{10}$	72	277.02 <sup>c</sup>	18.39 <sup>c</sup>	$2.36 \times 10^{11c}$	109	540.37 <sup>c</sup>	22.83 <sup>c</sup>	$1.08 \times 10^{12c}$
36	114.82	14.07 <sup>c</sup>	$2.22 \times 10^{10}$	73	283.06 <sup>c</sup>	18.51 <sup>c</sup>	$2.48 \times 10^{11c}$	110	548.63 <sup>c</sup>	22.95 <sup>c</sup>	$1.11 \times 10^{12c}$
37	118.54	14.19 <sup>c</sup>	$2.42 \times 10^{10}$	74	289.16 <sup>c</sup>	18.63 <sup>c</sup>	$2.60 \times 10^{11c}$	111	556.94 <sup>c</sup>	23.07 <sup>c</sup>	$1.15 \times 10^{12c}$
38	122.27	14.31 <sup>c</sup>	$2.64 \times 10^{10}$	75	295.31 <sup>c</sup>	18.75 <sup>c</sup>	$2.73 \times 10^{11c}$	112	565.32 <sup>c</sup>	23.19 <sup>c</sup>	$1.19 \times 10^{12c}$
39	126.00	14.43 <sup>c</sup>	$2.87 \times 10^{10}$	76	301.53 <sup>c</sup>	18.87 <sup>c</sup>	$2.87 \times 10^{11c}$	113	573.76 <sup>c</sup>	23.31 <sup>c</sup>	$1.23 \times 10^{12c}$
40	129.74	14.55 <sup>c</sup>	$3.11 \times 10^{10}$	77	307.81 <sup>c</sup>	18.99 <sup>c</sup>	$3.01 \times 10^{11c}$	114	582.26 <sup>c</sup>	23.43 <sup>c</sup>	$1.27 \times 10^{12c}$
41	133.47	14.67 <sup>c</sup>	$3.37 \times 10^{10}$	78	314.15 <sup>c</sup>	19.11 <sup>c</sup>	$3.15 \times 10^{11c}$	115	590.81 <sup>c</sup>	23.55 <sup>c</sup>	$1.31 \times 10^{12c}$
42	137.20	14.79 <sup>c</sup>	$3.64 \times 10^{10}$	79	320.54 <sup>c</sup>	19.23 <sup>c</sup>	$3.30 \times 10^{11c}$	116	599.43 <sup>c</sup>	23.67 <sup>c</sup>	$1.36 \times 10^{12c}$
43	140.93	14.91 <sup>c</sup>	$3.92 \times 10^{10}$	80	327.00 <sup>c</sup>	19.35 <sup>c</sup>	$3.46 \times 10^{11c}$	117	608.11 <sup>c</sup>	23.79 <sup>c</sup>	$1.40 \times 10^{12c}$
44	144.67	15.03 <sup>c</sup>	$4.22 \times 10^{10}$	81	333.52 <sup>c</sup>	19.47 <sup>c</sup>	$3.62 \times 10^{11c}$	118	616.85 <sup>c</sup>	23.91 <sup>c</sup>	$1.45 \times 10^{12c}$
45	148.40	15.15 <sup>c</sup>	$4.53 \times 10^{10}$	82	340.09 <sup>c</sup>	19.59 <sup>c</sup>	$3.78 \times 10^{11c}$	119	625.64 <sup>c</sup>	24.03 <sup>c</sup>	$1.49 \times 10^{12c}$
46	152.14	15.27 <sup>c</sup>	$4.85 \times 10^{10}$	83	346.73 <sup>c</sup>	19.71 <sup>c</sup>	$3.95 \times 10^{11c}$	120	634.50 <sup>c</sup>	24.15 <sup>c</sup>	$1.54 \times 10^{12c}$

<sup>a</sup> Reactions are based on point bearing at span ends.

<sup>b</sup> To obtain deflection for one wheel line in inches, divide the deflection coefficient by EI (lb-in<sup>3</sup>).

<sup>c</sup> Controlled by lane load rather than truck load.

Table 16-8. - Maximum vehicle moment, reaction, and deflection coefficient. Simple span, one wheel line, impact factor not included (*continued*).

Vehicle type H 20-44

Span (ft)	Moment (ft-kips)	Reaction <sup>a</sup> (kips)	Deflection <sup>b</sup> coefficient	Span (ft)	Moment (ft-kips)	Reaction <sup>a</sup> (kips)	Deflection <sup>b</sup> coefficient	Span (ft)	Moment (ft-kips)	Reaction <sup>a</sup> (kips)	Deflection <sup>b</sup> coefficient
10	40.00	16.00	$5.76 \times 10^3$	47	207.83	20.52 <sup>c</sup>	$6.92 \times 10^{10}$	84	471.24 <sup>c</sup>	26.44 <sup>c</sup>	$5.51 \times 10^{12}$
11	44.00	16.00	$7.67 \times 10^3$	48	212.82	20.68 <sup>c</sup>	$7.40 \times 10^{10}$	85	480.25 <sup>c</sup>	26.60 <sup>c</sup>	$5.75 \times 10^{12}$
12	48.00	16.00	$9.95 \times 10^3$	49	217.80	20.84 <sup>c</sup>	$7.89 \times 10^{10}$	86	489.34 <sup>c</sup>	26.76 <sup>c</sup>	$6.00 \times 10^{12}$
13	52.00	16.00	$1.27 \times 10^4$	50	222.78	21.00 <sup>c</sup>	$8.41 \times 10^{10}$	87	498.51 <sup>c</sup>	26.92 <sup>c</sup>	$6.26 \times 10^{12}$
14	56.00	16.00	$1.58 \times 10^4$	51	227.77	21.16 <sup>c</sup>	$8.95 \times 10^{10}$	88	507.76 <sup>c</sup>	27.08 <sup>c</sup>	$6.53 \times 10^{12}$
15	60.00	16.27	$1.94 \times 10^4$	52	232.75	21.32 <sup>c</sup>	$9.51 \times 10^{10}$	89	517.09 <sup>c</sup>	27.24 <sup>c</sup>	$6.80 \times 10^{12}$
16	64.00	16.50	$2.36 \times 10^4$	53	237.74	21.48 <sup>c</sup>	$1.01 \times 10^{11}$	90	526.50 <sup>c</sup>	27.40 <sup>c</sup>	$7.86 \times 10^{12}$
17	68.00	16.71	$2.83 \times 10^4$	54	242.73	21.64 <sup>c</sup>	$1.07 \times 10^{11}$	91	535.99 <sup>c</sup>	27.56 <sup>c</sup>	$7.38 \times 10^{12}$
18	72.00	16.89	$3.36 \times 10^4$	55	247.71	21.80 <sup>c</sup>	$1.13 \times 10^{11}$	92	545.56 <sup>c</sup>	27.72 <sup>c</sup>	$7.68 \times 10^{12}$
19	76.00	17.05	$3.95 \times 10^4$	56	252.70	21.96 <sup>c</sup>	$1.20 \times 10^{11}$	93	555.21 <sup>c</sup>	27.88 <sup>c</sup>	$7.99 \times 10^{12}$
20	80.00	17.20	$4.61 \times 10^4$	57	258.21 <sup>c</sup>	22.12 <sup>c</sup>	$1.36 \times 10^{11}$	94	564.94 <sup>c</sup>	28.04 <sup>c</sup>	$8.31 \times 10^{12}$
21	84.00	17.33	$5.33 \times 10^4$	58	265.06 <sup>c</sup>	22.28 <sup>c</sup>	$1.45 \times 10^{11}$	95	574.75 <sup>c</sup>	28.20 <sup>c</sup>	$8.64 \times 10^{12}$
22	88.00	17.45	$6.13 \times 10^4$	59	271.99 <sup>c</sup>	22.44 <sup>c</sup>	$1.54 \times 10^{11}$	96	584.64 <sup>c</sup>	28.36 <sup>c</sup>	$8.98 \times 10^{12}$
23	92.00	17.57	$7.01 \times 10^4$	60	279.00 <sup>c</sup>	22.60 <sup>c</sup>	$1.63 \times 10^{11}$	97	594.61 <sup>c</sup>	28.52 <sup>c</sup>	$9.33 \times 10^{12}$
24	96.00	17.67	$7.96 \times 10^4$	61	286.09 <sup>c</sup>	22.76 <sup>c</sup>	$1.73 \times 10^{11}$	98	604.66 <sup>c</sup>	28.68 <sup>c</sup>	$9.69 \times 10^{12}$
25	100.00	17.76	$9.00 \times 10^4$	62	293.26 <sup>c</sup>	22.92 <sup>c</sup>	$1.84 \times 10^{11}$	99	614.79 <sup>c</sup>	28.84 <sup>c</sup>	$1.01 \times 10^{13}$
26	104.00	17.85	$1.01 \times 10^{10}$	63	300.51 <sup>c</sup>	23.08 <sup>c</sup>	$1.94 \times 10^{11}$	100	625.00 <sup>c</sup>	29.00 <sup>c</sup>	$1.04 \times 10^{13}$
27	108.45	17.93	$1.14 \times 10^{10}$	64	307.84 <sup>c</sup>	23.24 <sup>c</sup>	$2.06 \times 10^{11}$	101	635.29 <sup>c</sup>	29.16 <sup>c</sup>	$1.08 \times 10^{13}$
28	113.40	18.00	$1.29 \times 10^{10}$	65	315.25 <sup>c</sup>	23.40 <sup>c</sup>	$2.18 \times 10^{11}$	102	645.66 <sup>c</sup>	29.32 <sup>c</sup>	$1.12 \times 10^{13}$
29	118.35	18.07	$1.45 \times 10^{10}$	66	322.74 <sup>c</sup>	23.56 <sup>c</sup>	$2.30 \times 10^{11}$	103	656.11 <sup>c</sup>	29.48 <sup>c</sup>	$1.16 \times 10^{13}$
30	123.31	18.13	$1.62 \times 10^{10}$	67	330.31 <sup>c</sup>	23.72 <sup>c</sup>	$2.43 \times 10^{11}$	104	666.64 <sup>c</sup>	29.64 <sup>c</sup>	$1.21 \times 10^{13}$
31	128.26	18.19	$1.81 \times 10^{10}$	68	337.96 <sup>c</sup>	23.88 <sup>c</sup>	$2.56 \times 10^{11}$	105	677.25 <sup>c</sup>	29.80 <sup>c</sup>	$1.25 \times 10^{13}$
32	133.23	18.25	$2.01 \times 10^{10}$	69	345.69 <sup>c</sup>	24.04 <sup>c</sup>	$2.70 \times 10^{11}$	106	687.94 <sup>c</sup>	29.96 <sup>c</sup>	$1.29 \times 10^{13}$
33	138.19	18.30	$2.23 \times 10^{10}$	70	353.50 <sup>c</sup>	24.20 <sup>c</sup>	$2.84 \times 10^{11}$	107	698.71 <sup>c</sup>	30.12 <sup>c</sup>	$1.34 \times 10^{13}$
34	143.15	18.44 <sup>c</sup>	$2.46 \times 10^{10}$	71	361.39 <sup>c</sup>	24.36 <sup>c</sup>	$2.99 \times 10^{11}$	108	709.56 <sup>c</sup>	30.28 <sup>c</sup>	$1.39 \times 10^{13}$
35	148.12	18.60 <sup>c</sup>	$2.70 \times 10^{10}$	72	369.36 <sup>c</sup>	24.52 <sup>c</sup>	$3.14 \times 10^{11}$	109	720.49 <sup>c</sup>	30.44 <sup>c</sup>	$1.44 \times 10^{13}$
36	153.09	18.76 <sup>c</sup>	$2.96 \times 10^{10}$	73	377.41 <sup>c</sup>	24.68 <sup>c</sup>	$3.31 \times 10^{11}$	110	731.50 <sup>c</sup>	30.60 <sup>c</sup>	$1.49 \times 10^{13}$
37	158.06	18.92 <sup>c</sup>	$3.23 \times 10^{10}$	74	385.54 <sup>c</sup>	24.84 <sup>c</sup>	$3.47 \times 10^{11}$	111	742.59 <sup>c</sup>	30.76 <sup>c</sup>	$1.54 \times 10^{13}$
38	163.03	19.08 <sup>c</sup>	$3.52 \times 10^{10}$	75	393.75 <sup>c</sup>	25.00 <sup>c</sup>	$3.65 \times 10^{11}$	112	753.76 <sup>c</sup>	30.92 <sup>c</sup>	$1.59 \times 10^{13}$
39	168.01	19.24 <sup>c</sup>	$3.83 \times 10^{10}$	76	402.04 <sup>c</sup>	25.16 <sup>c</sup>	$3.82 \times 10^{11}$	113	765.01 <sup>c</sup>	31.08 <sup>c</sup>	$1.64 \times 10^{13}$
40	172.98	19.40 <sup>c</sup>	$4.15 \times 10^{10}$	77	410.41 <sup>c</sup>	25.32 <sup>c</sup>	$4.01 \times 10^{11}$	114	776.34 <sup>c</sup>	31.24 <sup>c</sup>	$1.70 \times 10^{13}$
41	177.96	19.56 <sup>c</sup>	$4.49 \times 10^{10}$	78	418.86 <sup>c</sup>	25.48 <sup>c</sup>	$4.20 \times 10^{11}$	115	787.75 <sup>c</sup>	31.40 <sup>c</sup>	$1.75 \times 10^{13}$
42	182.93	19.72 <sup>c</sup>	$4.85 \times 10^{10}$	79	427.39 <sup>c</sup>	25.64 <sup>c</sup>	$4.40 \times 10^{11}$	116	799.24 <sup>c</sup>	31.56 <sup>c</sup>	$1.81 \times 10^{13}$
43	187.91	19.88 <sup>c</sup>	$5.23 \times 10^{10}$	80	436.00 <sup>c</sup>	25.80 <sup>c</sup>	$4.61 \times 10^{11}$	117	810.81 <sup>c</sup>	31.72 <sup>c</sup>	$1.87 \times 10^{13}$
44	192.89	20.04 <sup>c</sup>	$5.62 \times 10^{10}$	81	444.69 <sup>c</sup>	25.96 <sup>c</sup>	$4.82 \times 10^{11}$	118	822.46 <sup>c</sup>	31.88 <sup>c</sup>	$1.93 \times 10^{13}$
45	197.87	20.20 <sup>c</sup>	$6.04 \times 10^{10}$	82	453.46 <sup>c</sup>	26.12 <sup>c</sup>	$5.04 \times 10^{11}$	119	834.19 <sup>c</sup>	32.04 <sup>c</sup>	$1.99 \times 10^{13}$
46	202.85	20.36 <sup>c</sup>	$6.47 \times 10^{10}$	83	462.31 <sup>c</sup>	26.28 <sup>c</sup>	$5.27 \times 10^{11}$	120	846.00 <sup>c</sup>	32.20 <sup>c</sup>	$2.05 \times 10^{13}$

<sup>a</sup> Reactions are based on point bearing at span ends.

<sup>b</sup> To obtain deflection for one wheel line in inches, divide the deflection coefficient by EI (lb-in<sup>3</sup>).

<sup>c</sup> Controlled by lane load rather than truck load.

Table 16-8. - Maximum vehicle moment, reaction, and deflection coefficient. Simple span, one wheel line, impact factor not included (*continued*).

Vehicle type HS 15-44

Span (ft)	Moment (ft-kips)	Reaction <sup>a</sup> (kips)	Deflection <sup>b</sup> coefficient	Span (ft)	Moment (ft-kips)	Reaction <sup>a</sup> (kips)	Deflection <sup>b</sup> coefficient	Span (ft)	Moment (ft-kips)	Reaction <sup>a</sup> (kips)	Deflection <sup>b</sup> coefficient
10	30.00	12.00	$4.32 \times 10^4$	47	215.38	21.64	$8.14 \times 10^{10}$	84	463.75	24.00	$5.38 \times 10^{11}$
11	33.00	12.00	$5.75 \times 10^4$	48	222.06	21.75	$8.75 \times 10^{10}$	85	470.48	24.04	$5.58 \times 10^{11}$
12	36.00	12.00	$7.46 \times 10^4$	49	228.75	21.86	$9.39 \times 10^{10}$	86	477.21	24.07	$5.79 \times 10^{11}$
13	39.00	12.00	$9.49 \times 10^4$	50	235.44	21.96	$1.00 \times 10^{11}$	87	483.94	24.10	$6.00 \times 10^{11}$
14	42.00	12.00	$1.19 \times 10^5$	51	242.13	22.06	$1.07 \times 10^{11}$	88	490.67	24.14	$6.22 \times 10^{11}$
15	45.00	12.80	$1.46 \times 10^5$	52	248.83	22.15	$1.15 \times 10^{11}$	89	497.40	24.17	$6.44 \times 10^{11}$
16	48.00	13.50	$1.77 \times 10^5$	53	255.52	22.25	$1.22 \times 10^{11}$	90	504.13	24.20	$6.67 \times 10^{11}$
17	51.00	14.12	$2.12 \times 10^5$	54	262.22	22.33	$1.30 \times 10^{11}$	91	510.87	24.23	$6.91 \times 10^{11}$
18	54.00	14.67	$2.52 \times 10^5$	55	268.92	22.42	$1.38 \times 10^{11}$	92	517.60	24.26	$7.15 \times 10^{11}$
19	57.00	15.16	$2.98 \times 10^5$	56	275.63	22.50	$1.47 \times 10^{11}$	93	524.33	24.29	$7.39 \times 10^{11}$
20	60.00	15.60	$3.46 \times 10^5$	57	282.33	22.58	$1.55 \times 10^{11}$	94	531.06	24.32	$7.64 \times 10^{11}$
21	63.00	16.00	$4.00 \times 10^5$	58	289.03	22.66	$1.65 \times 10^{11}$	95	537.80	24.35	$7.90 \times 10^{11}$
22	66.00	16.36	$4.80 \times 10^5$	59	295.74	22.73	$1.74 \times 10^{11}$	96	544.53	24.38	$8.16 \times 10^{11}$
23	69.00	16.70	$5.86 \times 10^5$	60	302.45	22.80	$1.84 \times 10^{11}$	97	551.27	24.40	$8.42 \times 10^{11}$
24	72.25	17.00	$7.03 \times 10^5$	61	309.16	22.87	$1.94 \times 10^{11}$	98	558.00	24.43	$8.69 \times 10^{11}$
25	77.76	17.28	$8.34 \times 10^5$	62	315.87	22.94	$2.05 \times 10^{11}$	99	564.73	24.45	$8.97 \times 10^{11}$
26	83.31	17.54	$9.77 \times 10^5$	63	322.58	23.00	$2.15 \times 10^{11}$	100	571.47	24.48	$9.26 \times 10^{11}$
27	88.89	17.78	$1.13 \times 10^{10}$	64	329.30	23.06	$2.27 \times 10^{11}$	101	578.21	24.50	$9.55 \times 10^{11}$
28	94.50	18.00	$1.30 \times 10^{10}$	65	336.01	23.12	$2.38 \times 10^{11}$	102	584.94	24.53	$9.84 \times 10^{11}$
29	100.14	18.31	$1.49 \times 10^{10}$	66	342.73	23.18	$2.50 \times 10^{11}$	103	591.68	24.55	$1.01 \times 10^{12}$
30	105.80	18.60	$1.69 \times 10^{10}$	67	349.44	23.24	$2.63 \times 10^{11}$	104	598.41	24.58	$1.04 \times 10^{12}$
31	111.48	18.87	$1.91 \times 10^{10}$	68	356.16	23.29	$2.75 \times 10^{11}$	105	605.15	24.60	$1.08 \times 10^{12}$
32	117.19	19.13	$2.14 \times 10^{10}$	69	362.88	23.35	$2.89 \times 10^{11}$	106	611.89	24.62	$1.11 \times 10^{12}$
33	122.91	19.36	$2.39 \times 10^{10}$	70	369.60	23.40	$3.02 \times 10^{11}$	107	618.62	24.64	$1.14 \times 10^{12}$
34	128.82	19.59	$2.65 \times 10^{10}$	71	376.32	23.45	$3.16 \times 10^{11}$	108	625.38	24.67	$1.17 \times 10^{12}$
35	135.45	19.80	$2.93 \times 10^{10}$	72	383.04	23.50	$3.31 \times 10^{11}$	109	632.10	24.69	$1.21 \times 10^{12}$
36	142.08	20.00	$3.24 \times 10^{10}$	73	389.76	23.55	$3.45 \times 10^{11}$	110	638.84	24.71	$1.24 \times 10^{12}$
37	148.72	20.19	$3.56 \times 10^{10}$	74	396.49	23.59	$3.61 \times 10^{11}$	111	645.57	24.73	$1.28 \times 10^{12}$
38	155.37	20.37	$3.89 \times 10^{10}$	75	403.21	23.64	$3.76 \times 10^{11}$	112	652.31	24.75	$1.31 \times 10^{12}$
39	162.02	20.54	$4.25 \times 10^{10}$	76	409.93	23.68	$3.92 \times 10^{11}$	113	659.05	24.77	$1.35 \times 10^{12}$
40	168.68	20.70	$4.63 \times 10^{10}$	77	416.66	23.73	$4.09 \times 10^{11}$	114	665.79	24.79	$1.39 \times 10^{12}$
41	175.34	20.85	$5.06 \times 10^{10}$	78	423.38	23.77	$4.26 \times 10^{11}$	115	672.53	24.81	$1.42 \times 10^{12}$
42	182.00	21.00	$5.51 \times 10^{10}$	79	430.11	23.81	$4.43 \times 10^{11}$	116	679.27	24.83	$1.46 \times 10^{12}$
43	188.67	21.14	$5.98 \times 10^{10}$	80	436.84	23.85	$4.61 \times 10^{11}$	117	686.01	24.85	$1.50 \times 10^{12}$
44	195.34	21.27	$6.48 \times 10^{10}$	81	443.56	23.89	$4.80 \times 10^{11}$	118	692.75	24.86	$1.54 \times 10^{12}$
45	202.02	21.40	$7.01 \times 10^{10}$	82	450.29	23.93	$4.99 \times 10^{11}$	119	699.49	24.88	$1.58 \times 10^{12}$
46	208.70	21.52	$7.56 \times 10^{10}$	83	457.02	23.96	$5.18 \times 10^{11}$	120	706.23	24.90	$1.62 \times 10^{12}$

<sup>a</sup> Reactions are based on point bearing at span ends.

<sup>b</sup> To obtain deflection for one wheel line in inches, divide the deflection coefficient by EI (lb-in<sup>4</sup>).

<sup>c</sup> Truck loads control for all spans shown.

Table 16-8. - Maximum vehicle moment, reaction, and deflection coefficient. Simple span, one wheel line, impact factor not included (*continued*).

Vehicle type HS 20-44

Span (ft)	Moment (ft-kips)	Reaction <sup>a</sup> (kips)	Deflection <sup>b</sup> coefficient	Span (ft)	Moment (ft-kips)	Reaction <sup>a</sup> (kips)	Deflection <sup>b</sup> coefficient	Span (ft)	Moment (ft-kips)	Reaction <sup>a</sup> (kips)	Deflection <sup>b</sup> coefficient
10	40.00	16.00	$5.76 \times 10^6$	47	287.17	28.85	$1.09 \times 10^{11}$	84	618.33	32.00	$7.17 \times 10^{11}$
11	44.00	16.00	$7.67 \times 10^6$	48	296.08	29.00	$1.17 \times 10^{11}$	85	627.31	32.05	$7.44 \times 10^{11}$
12	48.00	16.00	$9.95 \times 10^6$	49	305.00	29.14	$1.25 \times 10^{11}$	86	636.28	32.09	$7.72 \times 10^{11}$
13	52.00	16.00	$1.27 \times 10^7$	50	313.92	29.28	$1.34 \times 10^{11}$	87	645.25	32.14	$8.00 \times 10^{11}$
14	56.00	16.00	$1.58 \times 10^7$	51	322.84	29.41	$1.43 \times 10^{11}$	88	654.23	32.18	$8.29 \times 10^{11}$
15	60.00	17.07	$1.94 \times 10^7$	52	331.77	29.54	$1.53 \times 10^{11}$	89	663.20	32.22	$8.59 \times 10^{11}$
16	64.00	18.00	$2.36 \times 10^7$	53	340.70	29.66	$1.63 \times 10^{11}$	90	672.18	32.27	$8.90 \times 10^{11}$
17	68.00	18.82	$2.83 \times 10^7$	54	349.63	29.78	$1.73 \times 10^{11}$	91	681.15	32.31	$9.21 \times 10^{11}$
18	72.00	19.56	$3.36 \times 10^7$	55	358.56	29.89	$1.84 \times 10^{11}$	92	690.13	32.35	$9.53 \times 10^{11}$
19	76.00	20.21	$3.95 \times 10^7$	56	367.50	30.00	$1.96 \times 10^{11}$	93	699.11	32.39	$9.85 \times 10^{11}$
20	80.00	20.80	$4.61 \times 10^7$	57	376.44	30.11	$2.07 \times 10^{11}$	94	708.09	32.43	$1.02 \times 10^{12}$
21	84.00	21.33	$5.33 \times 10^7$	58	385.38	30.21	$2.19 \times 10^{11}$	95	717.06	32.48	$1.05 \times 10^{12}$
22	88.00	21.82	$6.40 \times 10^7$	59	394.32	30.31	$2.32 \times 10^{11}$	96	726.04	32.50	$1.09 \times 10^{12}$
23	92.00	22.26	$7.81 \times 10^7$	60	403.27	30.40	$2.45 \times 10^{11}$	97	735.02	32.54	$1.12 \times 10^{12}$
24	96.33	22.67	$9.38 \times 10^7$	61	412.21	30.49	$2.59 \times 10^{11}$	98	744.00	32.57	$1.16 \times 10^{12}$
25	103.68	23.04	$1.11 \times 10^{10}$	62	421.16	30.58	$2.73 \times 10^{11}$	99	752.98	32.61	$1.20 \times 10^{12}$
26	111.08	23.38	$1.30 \times 10^{10}$	63	430.11	30.67	$2.87 \times 10^{11}$	100	761.96	32.64	$1.23 \times 10^{12}$
27	118.52	23.70	$1.51 \times 10^{10}$	64	439.06	30.75	$3.02 \times 10^{11}$	101	770.94	32.67	$1.27 \times 10^{12}$
28	126.00	24.00	$1.74 \times 10^{10}$	65	448.02	30.83	$3.18 \times 10^{11}$	102	779.92	32.71	$1.31 \times 10^{12}$
29	133.52	24.41	$1.99 \times 10^{10}$	66	456.97	30.91	$3.34 \times 10^{11}$	103	788.90	32.74	$1.35 \times 10^{12}$
30	141.07	24.80	$2.25 \times 10^{10}$	67	465.93	30.99	$3.50 \times 10^{11}$	104	797.88	32.77	$1.39 \times 10^{12}$
31	148.65	25.16	$2.54 \times 10^{10}$	68	474.88	31.06	$3.67 \times 10^{11}$	105	806.87	32.80	$1.44 \times 10^{12}$
32	156.25	25.50	$2.85 \times 10^{10}$	69	483.84	31.13	$3.85 \times 10^{11}$	106	815.85	32.83	$1.48 \times 10^{12}$
33	163.88	25.82	$3.18 \times 10^{10}$	70	492.80	31.20	$4.03 \times 10^{11}$	107	824.83	32.86	$1.52 \times 10^{12}$
34	171.76	26.12	$3.53 \times 10^{10}$	71	501.76	31.27	$4.22 \times 10^{11}$	108	833.81	32.89	$1.57 \times 10^{12}$
35	180.60	26.40	$3.91 \times 10^{10}$	72	510.72	31.33	$4.41 \times 10^{11}$	109	842.80	32.92	$1.61 \times 10^{12}$
36	189.44	26.67	$4.31 \times 10^{10}$	73	519.68	31.40	$4.61 \times 10^{11}$	110	851.78	32.95	$1.66 \times 10^{12}$
37	198.30	26.92	$4.74 \times 10^{10}$	74	528.65	31.46	$4.81 \times 10^{11}$	111	860.77	32.97	$1.70 \times 10^{12}$
38	207.16	27.16	$5.19 \times 10^{10}$	75	537.61	31.52	$5.02 \times 10^{11}$	112	869.75	33.00	$1.75 \times 10^{12}$
39	216.03	27.38	$5.67 \times 10^{10}$	76	546.58	31.58	$5.23 \times 10^{11}$	113	878.73	33.03	$1.80 \times 10^{12}$
40	224.90	27.60	$6.18 \times 10^{10}$	77	555.55	31.64	$5.45 \times 10^{11}$	114	887.72	33.05	$1.85 \times 10^{12}$
41	233.78	27.80	$6.74 \times 10^{10}$	78	564.51	31.69	$5.68 \times 10^{11}$	115	896.70	33.08	$1.90 \times 10^{12}$
42	242.67	28.00	$7.34 \times 10^{10}$	79	573.48	31.75	$5.91 \times 10^{11}$	116	905.69	33.10	$1.95 \times 10^{12}$
43	251.56	28.19	$7.98 \times 10^{10}$	80	582.45	31.80	$6.15 \times 10^{11}$	117	914.68	33.13	$2.00 \times 10^{12}$
44	260.45	28.36	$8.65 \times 10^{10}$	81	591.42	31.85	$6.40 \times 10^{11}$	118	923.68	33.15	$2.06 \times 10^{12}$
45	269.36	28.53	$9.35 \times 10^{10}$	82	600.39	31.90	$6.65 \times 10^{11}$	119	932.65	33.18	$2.11 \times 10^{12}$
46	278.26	28.70	$1.01 \times 10^{11}$	83	609.36	31.95	$6.91 \times 10^{11}$	120	941.63	33.20	$2.16 \times 10^{12}$

<sup>a</sup> Reactions are based on point bearing at span ends.

<sup>b</sup> To obtain deflection for one wheel line in inches, divide the deflection coefficient by  $EI$  (lb-in<sup>2</sup>).

<sup>c</sup> Truck loads control for all spans shown.

Table 16-8. - Maximum vehicle moment, reaction, and deflection coefficient. Simple span, one wheel line, impact factor not included (*continued*).

Vehicle type HS 25-44

Span (ft)	Moment (ft-kips)	Reaction <sup>a</sup> (kips)	Deflection <sup>b</sup> coefficient	Span (ft)	Moment (ft-kips)	Reaction <sup>a</sup> (kips)	Deflection <sup>b</sup> coefficient	Span (ft)	Moment (ft-kips)	Reaction <sup>a</sup> (kips)	Deflection <sup>b</sup> coefficient
10	50.00	20.00	$7.20 \times 10^9$	47	358.96	36.06	$1.36 \times 10^{11}$	84	772.92	40.00	$8.96 \times 10^{11}$
11	55.00	20.00	$9.58 \times 10^9$	48	370.10	36.25	$1.46 \times 10^{11}$	85	784.13	40.06	$9.30 \times 10^{11}$
12	60.00	20.00	$1.24 \times 10^{10}$	49	381.25	36.43	$1.56 \times 10^{11}$	86	795.35	40.12	$9.65 \times 10^{11}$
13	65.00	20.00	$1.58 \times 10^{10}$	50	392.40	36.60	$1.67 \times 10^{11}$	87	806.57	40.17	$1.00 \times 10^{12}$
14	70.00	20.00	$1.98 \times 10^{10}$	51	403.55	36.76	$1.79 \times 10^{11}$	88	817.78	40.23	$1.04 \times 10^{12}$
15	75.00	21.33	$2.43 \times 10^{10}$	52	414.71	36.92	$1.91 \times 10^{11}$	89	829.00	40.28	$1.07 \times 10^{12}$
16	80.00	22.50	$2.95 \times 10^{10}$	53	425.87	37.08	$2.04 \times 10^{11}$	90	840.22	40.33	$1.11 \times 10^{12}$
17	85.00	23.53	$3.54 \times 10^{10}$	54	437.04	37.22	$2.17 \times 10^{11}$	91	851.44	40.38	$1.15 \times 10^{12}$
18	90.00	24.44	$4.20 \times 10^{10}$	55	448.20	37.36	$2.30 \times 10^{11}$	92	862.66	40.43	$1.19 \times 10^{12}$
19	95.00	25.26	$4.94 \times 10^{10}$	56	459.38	37.50	$2.44 \times 10^{11}$	93	873.88	40.48	$1.23 \times 10^{12}$
20	100.00	26.00	$5.76 \times 10^{10}$	57	470.55	37.63	$2.59 \times 10^{11}$	94	885.11	40.53	$1.27 \times 10^{12}$
21	105.00	26.67	$6.67 \times 10^{10}$	58	481.72	37.76	$2.74 \times 10^{11}$	95	896.33	40.58	$1.32 \times 10^{12}$
22	110.00	27.27	$7.99 \times 10^{10}$	59	492.90	37.88	$2.90 \times 10^{11}$	96	907.55	40.63	$1.36 \times 10^{12}$
23	115.00	27.83	$9.76 \times 10^{10}$	60	504.08	38.00	$3.06 \times 10^{11}$	97	918.78	40.67	$1.40 \times 10^{12}$
24	120.42	28.33	$1.17 \times 10^{11}$	61	515.27	38.11	$3.23 \times 10^{11}$	98	930.00	40.71	$1.45 \times 10^{12}$
25	129.60	28.80	$1.39 \times 10^{11}$	62	526.45	38.23	$3.41 \times 10^{11}$	99	941.22	40.76	$1.50 \times 10^{12}$
26	138.85	29.23	$1.63 \times 10^{11}$	63	537.64	38.33	$3.59 \times 10^{11}$	100	952.45	40.80	$1.54 \times 10^{12}$
27	148.15	29.63	$1.89 \times 10^{11}$	64	548.83	38.44	$3.78 \times 10^{11}$	101	963.68	40.84	$1.59 \times 10^{12}$
28	157.50	30.00	$2.17 \times 10^{11}$	65	560.02	38.54	$3.97 \times 10^{11}$	102	974.90	40.88	$1.64 \times 10^{12}$
29	166.90	30.52	$2.48 \times 10^{11}$	66	571.21	38.64	$4.17 \times 10^{11}$	103	986.13	40.92	$1.69 \times 10^{12}$
30	176.33	31.00	$2.82 \times 10^{11}$	67	582.41	38.73	$4.38 \times 10^{11}$	104	997.36	40.96	$1.74 \times 10^{12}$
31	185.81	31.45	$3.18 \times 10^{11}$	68	593.60	38.82	$4.59 \times 10^{11}$	105	1,008.58	41.00	$1.79 \times 10^{12}$
32	195.31	31.88	$3.56 \times 10^{11}$	69	604.80	38.91	$4.81 \times 10^{11}$	106	1,019.81	41.04	$1.85 \times 10^{12}$
33	204.85	32.27	$3.98 \times 10^{11}$	70	616.00	39.00	$5.04 \times 10^{11}$	107	1,031.04	41.07	$1.90 \times 10^{12}$
34	214.71	32.65	$4.42 \times 10^{11}$	71	627.20	39.08	$5.27 \times 10^{11}$	108	1,042.27	41.11	$1.96 \times 10^{12}$
35	225.75	33.00	$4.89 \times 10^{11}$	72	638.40	39.17	$5.51 \times 10^{11}$	109	1,053.50	41.15	$2.01 \times 10^{12}$
36	236.81	33.33	$5.39 \times 10^{11}$	73	649.61	39.25	$5.76 \times 10^{11}$	110	1,064.73	41.18	$2.07 \times 10^{12}$
37	247.87	33.65	$5.93 \times 10^{11}$	74	660.81	39.32	$6.01 \times 10^{11}$	111	1,075.96	41.22	$2.13 \times 10^{12}$
38	258.95	33.95	$6.49 \times 10^{11}$	75	672.02	39.40	$6.27 \times 10^{11}$	112	1,087.19	41.25	$2.19 \times 10^{12}$
39	270.03	34.23	$7.09 \times 10^{11}$	76	683.22	39.47	$6.54 \times 10^{11}$	113	1,098.42	41.28	$2.25 \times 10^{12}$
40	281.13	34.50	$7.72 \times 10^{11}$	77	694.43	39.55	$6.82 \times 10^{11}$	114	1,109.65	41.32	$2.31 \times 10^{12}$
41	292.23	34.76	$8.43 \times 10^{11}$	78	705.64	39.62	$7.10 \times 10^{11}$	115	1,120.88	41.35	$2.37 \times 10^{12}$
42	303.33	35.00	$9.18 \times 10^{11}$	79	716.85	39.68	$7.39 \times 10^{11}$	116	1,132.11	41.38	$2.44 \times 10^{12}$
43	314.45	35.23	$9.97 \times 10^{11}$	80	728.06	39.75	$7.69 \times 10^{11}$	117	1,143.34	41.41	$2.50 \times 10^{12}$
44	325.57	35.45	$1.08 \times 10^{12}$	81	739.27	39.81	$8.00 \times 10^{11}$	118	1,154.58	41.44	$2.57 \times 10^{12}$
45	336.69	35.67	$1.17 \times 10^{12}$	82	750.49	39.88	$8.31 \times 10^{11}$	119	1,165.81	41.47	$2.64 \times 10^{12}$
46	347.83	35.87	$1.26 \times 10^{12}$	83	761.70	39.94	$8.63 \times 10^{11}$	120	1,177.04	41.50	$2.71 \times 10^{12}$

<sup>a</sup> Reactions are based on point bearing at span ends.

<sup>b</sup> To obtain deflection for one wheel line in inches, divide the deflection coefficient by EI (lb-in<sup>3</sup>).

<sup>c</sup> Truck loads control for all spans shown.

Table 16-8. - Maximum vehicle moment, reaction, and deflection coefficient. Simple span, one wheel line, impact factor not included (*continued*).

Vehicle type Alternate Military Loading

Span (ft)	Moment (ft-kips)	Reaction <sup>a</sup> (kips)	Deflection <sup>b</sup> coefficient	Span (ft)	Moment (ft-kips)	Reaction <sup>a</sup> (kips)	Deflection <sup>b</sup> coefficient	Span (ft)	Moment (ft-kips)	Reaction <sup>a</sup> (kips)	Deflection <sup>b</sup> coefficient
10	50.40	19.20	$6.84 \times 10^8$	47	270.51	22.98	$8.88 \times 10^{10}$	84	492.29	23.43	$5.10 \times 10^{11}$
11	56.18	19.64	$9.50 \times 10^8$	48	276.50	23.00	$9.46 \times 10^{10}$	85	498.28	23.44	$5.29 \times 10^{11}$
12	62.00	20.00	$1.27 \times 10^9$	49	282.49	23.02	$1.01 \times 10^{11}$	86	504.28	23.44	$5.48 \times 10^{11}$
13	67.85	20.31	$1.66 \times 10^9$	50	288.48	23.04	$1.07 \times 10^{11}$	87	510.28	23.45	$5.67 \times 10^{11}$
14	73.71	20.57	$2.11 \times 10^9$	51	294.47	23.06	$1.14 \times 10^{11}$	88	516.27	23.45	$5.87 \times 10^{11}$
15	79.60	20.80	$2.63 \times 10^9$	52	300.46	23.08	$1.20 \times 10^{11}$	89	522.27	23.46	$6.07 \times 10^{11}$
16	85.50	21.00	$3.23 \times 10^9$	53	306.45	23.09	$1.28 \times 10^{11}$	90	528.27	23.47	$6.28 \times 10^{11}$
17	91.41	21.18	$3.92 \times 10^9$	54	312.44	23.11	$1.35 \times 10^{11}$	91	534.26	23.47	$6.49 \times 10^{11}$
18	97.33	21.33	$4.69 \times 10^9$	55	318.44	23.13	$1.43 \times 10^{11}$	92	540.26	23.48	$6.71 \times 10^{11}$
19	103.26	21.47	$5.56 \times 10^9$	56	324.43	23.14	$1.51 \times 10^{11}$	93	546.26	23.48	$6.93 \times 10^{11}$
20	109.20	21.60	$6.52 \times 10^9$	57	330.42	23.16	$1.59 \times 10^{11}$	94	552.26	23.49	$7.16 \times 10^{11}$
21	115.14	21.71	$7.59 \times 10^9$	58	336.41	23.17	$1.67 \times 10^{11}$	95	558.25	23.49	$7.39 \times 10^{11}$
22	121.09	21.82	$8.77 \times 10^9$	59	342.41	23.19	$1.76 \times 10^{11}$	96	564.25	23.50	$7.62 \times 10^{11}$
23	127.04	21.91	$1.01 \times 10^{10}$	60	348.40	23.20	$1.85 \times 10^{11}$	97	570.25	23.51	$7.87 \times 10^{11}$
24	133.00	22.00	$1.15 \times 10^{10}$	61	354.39	23.21	$1.95 \times 10^{11}$	98	576.24	23.51	$8.11 \times 10^{11}$
25	138.96	22.08	$1.30 \times 10^{10}$	62	360.39	23.23	$2.05 \times 10^{11}$	99	582.24	23.52	$8.36 \times 10^{11}$
26	144.92	22.15	$1.47 \times 10^{10}$	63	366.38	23.24	$2.15 \times 10^{11}$	100	588.24	23.52	$8.62 \times 10^{11}$
27	150.89	22.22	$1.65 \times 10^{10}$	64	372.38	23.25	$2.25 \times 10^{11}$	101	594.24	23.52	$8.88 \times 10^{11}$
28	156.86	22.29	$1.84 \times 10^{10}$	65	378.37	23.26	$2.36 \times 10^{11}$	102	600.24	23.53	$9.15 \times 10^{11}$
29	162.83	22.34	$2.05 \times 10^{10}$	66	384.36	23.27	$2.47 \times 10^{11}$	103	606.23	23.53	$9.42 \times 10^{11}$
30	168.80	22.40	$2.27 \times 10^{10}$	67	390.36	23.28	$2.58 \times 10^{11}$	104	612.23	23.54	$9.70 \times 10^{11}$
31	174.77	22.45	$2.51 \times 10^{10}$	68	396.35	23.29	$2.70 \times 10^{11}$	105	618.23	23.54	$9.98 \times 10^{11}$
32	180.75	22.50	$2.77 \times 10^{10}$	69	402.35	23.30	$2.82 \times 10^{11}$	106	624.23	23.55	$1.03 \times 10^{12}$
33	186.73	22.55	$3.04 \times 10^{10}$	70	408.34	23.31	$2.95 \times 10^{11}$	107	630.22	23.55	$1.06 \times 10^{12}$
34	192.71	22.59	$3.33 \times 10^{10}$	71	414.34	23.32	$3.08 \times 10^{11}$	108	636.22	23.56	$1.09 \times 10^{12}$
35	198.69	22.63	$3.63 \times 10^{10}$	72	420.33	23.33	$3.21 \times 10^{11}$	109	642.22	23.56	$1.12 \times 10^{12}$
36	204.67	22.67	$3.96 \times 10^{10}$	73	426.33	23.34	$3.35 \times 10^{11}$	110	648.22	23.56	$1.15 \times 10^{12}$
37	210.65	22.70	$4.30 \times 10^{10}$	74	432.32	23.35	$3.49 \times 10^{11}$	111	654.22	23.57	$1.18 \times 10^{12}$
38	216.63	22.74	$4.66 \times 10^{10}$	75	438.32	23.36	$3.63 \times 10^{11}$	112	660.21	23.57	$1.21 \times 10^{12}$
39	222.62	22.77	$5.05 \times 10^{10}$	76	444.32	23.37	$3.78 \times 10^{11}$	113	666.21	23.58	$1.24 \times 10^{12}$
40	228.60	22.80	$5.45 \times 10^{10}$	77	450.31	23.38	$3.93 \times 10^{11}$	114	672.21	23.58	$1.28 \times 10^{12}$
41	234.59	22.83	$5.87 \times 10^{10}$	78	456.31	23.38	$4.08 \times 10^{11}$	115	678.21	23.58	$1.31 \times 10^{12}$
42	240.57	22.86	$6.32 \times 10^{10}$	79	462.30	23.39	$4.24 \times 10^{11}$	116	684.21	23.59	$1.35 \times 10^{12}$
43	246.56	22.88	$6.78 \times 10^{10}$	80	468.30	23.40	$4.41 \times 10^{11}$	117	690.21	23.59	$1.38 \times 10^{12}$
44	252.55	22.91	$7.27 \times 10^{10}$	81	474.30	23.41	$4.58 \times 10^{11}$	118	696.20	23.59	$1.42 \times 10^{12}$
45	258.53	22.93	$7.78 \times 10^{10}$	82	480.29	23.41	$4.75 \times 10^{11}$	119	702.20	23.60	$1.45 \times 10^{12}$
46	264.52	22.96	$8.32 \times 10^{10}$	83	486.29	23.42	$4.92 \times 10^{11}$	120	708.20	23.60	$1.49 \times 10^{12}$

<sup>a</sup> Reactions are based on point bearing at span ends.

<sup>b</sup> To obtain deflection for one wheel line in inches, divide the deflection coefficient by EI (lb-in<sup>3</sup>).



Table 16-8. - Maximum vehicle moment, reaction, and deflection coefficient. Simple span, one wheel line, impact factor not included (*continued*).

Vehicle type U80

Span (ft)	Moment (ft-kips)	Reaction <sup>a</sup> (kips)	Deflection <sup>b</sup> coefficient	Span (ft)	Moment (ft-kips)	Reaction <sup>a</sup> (kips)	Deflection <sup>b</sup> coefficient	Span (ft)	Moment (ft-kips)	Reaction <sup>a</sup> (kips)	Deflection <sup>b</sup> coefficient
10	55.56	28.68	$9.88 \times 10^8$	47	552.82	57.17	$2.18 \times 10^{11}$	84	1,287.94	67.23	$1.54 \times 10^{12}$
11	64.38	29.43	$1.39 \times 10^9$	48	572.59	57.65	$2.35 \times 10^{11}$	85	1,307.87	67.38	$1.60 \times 10^{12}$
12	73.28	30.06	$1.88 \times 10^9$	49	592.37	58.10	$2.52 \times 10^{11}$	86	1,327.80	67.52	$1.66 \times 10^{12}$
13	82.23	30.60	$2.46 \times 10^9$	50	612.15	58.54	$2.71 \times 10^{11}$	87	1,347.73	67.67	$1.72 \times 10^{12}$
14	91.22	31.05	$3.15 \times 10^9$	51	631.95	58.96	$2.91 \times 10^{11}$	88	1,367.66	67.81	$1.79 \times 10^{12}$
15	100.25	31.45	$3.95 \times 10^9$	52	651.75	59.37	$3.11 \times 10^{11}$	89	1,387.60	67.94	$1.85 \times 10^{12}$
16	109.30	31.80	$4.87 \times 10^9$	53	671.57	59.76	$3.33 \times 10^{11}$	90	1,407.53	68.08	$1.92 \times 10^{12}$
17	118.38	32.10	$5.92 \times 10^9$	54	691.38	60.13	$3.56 \times 10^{11}$	91	1,427.47	68.21	$1.99 \times 10^{12}$
18	127.48	32.38	$7.10 \times 10^9$	55	711.21	60.49	$3.79 \times 10^{11}$	92	1,447.40	68.34	$2.06 \times 10^{12}$
19	136.59	33.10	$8.43 \times 10^9$	56	731.04	60.84	$4.03 \times 10^{11}$	93	1,467.34	68.46	$2.13 \times 10^{12}$
20	145.72	34.22	$9.91 \times 10^9$	57	750.88	61.18	$4.29 \times 10^{11}$	94	1,487.28	68.59	$2.20 \times 10^{12}$
21	154.85	35.23	$1.15 \times 10^{10}$	58	770.72	61.50	$4.55 \times 10^{11}$	95	1,507.23	68.71	$2.28 \times 10^{12}$
22	164.00	36.15	$1.34 \times 10^{10}$	59	790.57	61.81	$4.82 \times 10^{11}$	96	1,527.17	68.82	$2.36 \times 10^{12}$
23	173.16	36.99	$1.53 \times 10^{10}$	60	810.42	62.12	$5.11 \times 10^{11}$	97	1,547.11	68.94	$2.43 \times 10^{12}$
24	182.33	38.54	$1.75 \times 10^{10}$	61	830.28	62.41	$5.40 \times 10^{11}$	98	1,567.06	69.05	$2.51 \times 10^{12}$
25	191.50	39.96	$1.99 \times 10^{10}$	62	850.14	62.69	$5.71 \times 10^{11}$	99	1,587.00	69.16	$2.60 \times 10^{12}$
26	200.68	41.27	$2.24 \times 10^{10}$	63	870.01	62.97	$6.02 \times 10^{11}$	100	1,606.95	69.27	$2.68 \times 10^{12}$
27	209.86	42.48	$2.52 \times 10^{10}$	64	889.88	63.24	$6.35 \times 10^{11}$	101	1,626.90	69.38	$2.76 \times 10^{12}$
28	222.34	43.61	$2.82 \times 10^{10}$	65	909.75	63.49	$6.68 \times 10^{11}$	102	1,646.85	69.48	$2.85 \times 10^{12}$
29	236.04	44.66	$3.29 \times 10^{10}$	66	929.63	63.74	$7.03 \times 10^{11}$	103	1,666.80	69.58	$2.94 \times 10^{12}$
30	249.76	45.63	$3.84 \times 10^{10}$	67	949.51	63.99	$7.39 \times 10^{11}$	104	1,686.75	69.68	$3.03 \times 10^{12}$
31	263.48	46.55	$4.44 \times 10^{10}$	68	969.40	64.22	$7.76 \times 10^{11}$	105	1,706.70	69.78	$3.12 \times 10^{12}$
32	278.08	47.41	$5.09 \times 10^{10}$	69	989.29	64.45	$8.15 \times 10^{11}$	106	1,726.66	69.88	$3.22 \times 10^{12}$
33	295.72	48.21	$5.79 \times 10^{10}$	70	1,009.18	64.67	$8.54 \times 10^{11}$	107	1,746.61	69.97	$3.31 \times 10^{12}$
34	313.41	48.97	$6.54 \times 10^{10}$	71	1,029.08	64.89	$8.95 \times 10^{11}$	108	1,766.57	70.07	$3.41 \times 10^{12}$
35	331.15	49.69	$7.35 \times 10^{10}$	72	1,048.98	65.10	$9.37 \times 10^{11}$	109	1,786.52	70.16	$3.51 \times 10^{12}$
36	348.93	50.36	$8.21 \times 10^{10}$	73	1,068.88	65.30	$9.80 \times 10^{11}$	110	1,806.48	70.25	$3.61 \times 10^{12}$
37	366.75	51.00	$9.13 \times 10^{10}$	74	1,088.78	65.50	$1.02 \times 10^{12}$	111	1,826.44	70.33	$3.71 \times 10^{12}$
38	384.61	51.76	$1.01 \times 10^{11}$	75	1,108.69	65.69	$1.07 \times 10^{12}$	112	1,846.40	70.42	$3.82 \times 10^{12}$
39	402.49	52.49	$1.11 \times 10^{11}$	76	1,128.60	65.88	$1.12 \times 10^{12}$	113	1,866.35	70.50	$3.93 \times 10^{12}$
40	420.41	53.18	$1.22 \times 10^{11}$	77	1,148.51	66.07	$1.17 \times 10^{12}$	114	1,886.31	70.59	$4.03 \times 10^{12}$
41	438.36	53.83	$1.34 \times 10^{11}$	78	1,168.42	66.24	$1.22 \times 10^{12}$	115	1,906.27	70.67	$4.15 \times 10^{12}$
42	456.33	54.45	$1.46 \times 10^{11}$	79	1,188.34	66.42	$1.27 \times 10^{12}$	116	1,926.23	70.75	$4.26 \times 10^{12}$
43	474.33	55.05	$1.59 \times 10^{11}$	80	1,208.25	66.59	$1.32 \times 10^{12}$	117	1,946.20	70.83	$4.37 \times 10^{12}$
44	493.57	55.61	$1.73 \times 10^{11}$	81	1,228.17	66.75	$1.37 \times 10^{12}$	118	1,966.16	70.91	$4.49 \times 10^{12}$
45	513.31	56.16	$1.88 \times 10^{11}$	82	1,248.09	66.92	$1.43 \times 10^{12}$	119	1,986.12	70.98	$4.61 \times 10^{12}$
46	533.06	56.67	$2.03 \times 10^{11}$	83	1,268.02	67.07	$1.48 \times 10^{12}$	120	2,006.09	71.06	$4.73 \times 10^{12}$

<sup>a</sup> Reactions are based on point bearing at span ends.

<sup>b</sup> To obtain deflection for one wheel line in inches, divide the deflection coefficient by EI (lb-in<sup>3</sup>).

Table 16-8. - Maximum vehicle moment, reaction, and deflection coefficient. Simple span, one wheel line, impact factor not included (*continued*).

Vehicle type U102

Span (ft)	Moment (ft-kips)	Reaction <sup>a</sup> (kips)	Deflection <sup>b</sup> coefficient	Span (ft)	Moment (ft-kips)	Reaction <sup>a</sup> (kips)	Deflection <sup>b</sup> coefficient	Span (ft)	Moment (ft-kips)	Reaction <sup>a</sup> (kips)	Deflection <sup>b</sup> coefficient
10	84.09	43.40	$1.50 \times 10^9$	47	596.51	54.45	$2.07 \times 10^{11}$	84	1,191.86	74.32	$1.39 \times 10^{12}$
11	97.44	44.55	$2.10 \times 10^9$	48	610.48	54.92	$2.20 \times 10^{11}$	85	1,215.49	74.65	$1.45 \times 10^{12}$
12	110.91	45.50	$2.84 \times 10^9$	49	624.45	55.38	$2.34 \times 10^{11}$	86	1,239.15	74.98	$1.52 \times 10^{12}$
13	124.45	46.31	$3.72 \times 10^9$	50	638.42	56.24	$2.49 \times 10^{11}$	87	1,262.83	75.29	$1.59 \times 10^{12}$
14	138.06	47.00	$3.77 \times 10^9$	51	652.39	57.07	$2.64 \times 10^{11}$	88	1,286.53	75.60	$1.66 \times 10^{12}$
15	151.72	47.60	$5.98 \times 10^9$	52	666.36	57.87	$2.80 \times 10^{11}$	89	1,310.25	75.91	$1.74 \times 10^{12}$
16	165.43	48.13	$7.37 \times 10^9$	53	680.34	58.63	$2.97 \times 10^{11}$	90	1,333.99	76.20	$1.81 \times 10^{12}$
17	179.17	48.59	$8.96 \times 10^{10}$	54	694.31	59.37	$3.14 \times 10^{11}$	91	1,357.75	76.49	$1.89 \times 10^{12}$
18	192.94	49.00	$1.07 \times 10^{10}$	55	708.29	60.08	$3.32 \times 10^{11}$	92	1,381.53	76.77	$1.97 \times 10^{12}$
19	206.73	49.37	$1.28 \times 10^{10}$	56	722.27	60.77	$3.51 \times 10^{11}$	93	1,405.33	77.05	$2.06 \times 10^{12}$
20	220.54	49.70	$1.50 \times 10^{10}$	57	736.24	61.43	$3.70 \times 10^{11}$	94	1,429.15	77.32	$2.14 \times 10^{12}$
21	234.37	50.00	$1.75 \times 10^{10}$	58	750.22	62.07	$3.90 \times 10^{11}$	95	1,452.98	77.59	$2.23 \times 10^{12}$
22	248.22	50.27	$2.02 \times 10^{10}$	59	764.20	62.69	$4.11 \times 10^{11}$	96	1,476.83	77.85	$2.32 \times 10^{12}$
23	262.08	50.52	$2.32 \times 10^{10}$	60	778.18	63.29	$4.32 \times 10^{11}$	97	1,500.69	78.10	$2.41 \times 10^{12}$
24	275.95	50.75	$2.65 \times 10^{10}$	61	792.16	63.86	$4.54 \times 10^{11}$	98	1,524.57	78.35	$2.50 \times 10^{12}$
25	289.83	50.96	$3.01 \times 10^{10}$	62	806.14	64.42	$4.77 \times 10^{11}$	99	1,548.47	78.59	$2.60 \times 10^{12}$
26	303.73	51.15	$3.39 \times 10^{10}$	63	820.12	64.96	$5.00 \times 10^{11}$	100	1,572.38	78.83	$2.70 \times 10^{12}$
27	317.62	51.33	$3.81 \times 10^{10}$	64	834.11	65.52	$5.25 \times 10^{11}$	101	1,596.65	79.07	$2.80 \times 10^{12}$
28	331.53	51.50	$4.26 \times 10^{10}$	65	848.09	66.09	$5.50 \times 10^{11}$	102	1,621.41	79.30	$2.90 \times 10^{12}$
29	345.44	51.66	$4.75 \times 10^{10}$	66	862.07	66.64	$5.76 \times 10^{11}$	103	1,646.20	79.52	$3.00 \times 10^{12}$
30	359.36	51.80	$5.27 \times 10^{10}$	67	876.06	67.17	$6.02 \times 10^{11}$	104	1,670.99	79.74	$3.11 \times 10^{12}$
31	373.29	51.94	$5.83 \times 10^{10}$	68	890.04	67.69	$6.30 \times 10^{11}$	105	1,695.81	79.96	$3.22 \times 10^{12}$
32	387.21	52.06	$6.41 \times 10^{10}$	69	904.03	68.20	$6.58 \times 10^{11}$	106	1,720.63	80.17	$3.33 \times 10^{12}$
33	401.15	52.18	$7.05 \times 10^{10}$	70	918.01	68.69	$6.87 \times 10^{11}$	107	1,745.48	80.38	$3.44 \times 10^{12}$
34	415.08	52.29	$7.72 \times 10^{10}$	71	932.00	69.16	$7.17 \times 10^{11}$	108	1,770.34	80.58	$3.56 \times 10^{12}$
35	429.02	52.40	$8.44 \times 10^{10}$	72	945.98	69.63	$7.48 \times 10^{11}$	109	1,795.21	80.79	$3.68 \times 10^{12}$
36	442.97	52.50	$9.19 \times 10^{10}$	73	959.97	70.08	$7.80 \times 10^{11}$	110	1,820.09	80.98	$3.80 \times 10^{12}$
37	456.92	52.59	$9.99 \times 10^{10}$	74	973.96	70.52	$8.25 \times 10^{11}$	111	1,844.99	81.18	$3.92 \times 10^{12}$
38	470.87	52.68	$1.08 \times 10^{11}$	75	987.94	70.94	$8.74 \times 10^{11}$	112	1,869.90	81.37	$4.05 \times 10^{12}$
39	484.82	52.77	$1.17 \times 10^{11}$	76	1,003.73	71.36	$9.24 \times 10^{11}$	113	1,894.83	81.55	$4.18 \times 10^{12}$
40	498.77	52.85	$1.27 \times 10^{11}$	77	1,027.14	71.76	$9.76 \times 10^{11}$	114	1,919.77	81.74	$4.31 \times 10^{12}$
41	512.73	52.93	$1.37 \times 10^{11}$	78	1,050.59	72.16	$1.03 \times 10^{12}$	115	1,944.71	81.92	$4.44 \times 10^{12}$
42	526.69	53.00	$1.47 \times 10^{11}$	79	1,074.07	72.54	$1.08 \times 10^{12}$	116	1,969.67	82.10	$4.58 \times 10^{12}$
43	540.65	53.07	$1.58 \times 10^{11}$	80	1,097.57	72.91	$1.14 \times 10^{12}$	117	1,994.65	82.27	$4.71 \times 10^{12}$
44	554.61	53.14	$1.69 \times 10^{11}$	81	1,121.10	73.28	$1.20 \times 10^{12}$	118	2,019.63	82.44	$4.85 \times 10^{12}$
45	568.57	53.44	$1.81 \times 10^{11}$	82	1,144.66	73.64	$1.26 \times 10^{12}$	119	2,044.62	82.61	$5.00 \times 10^{12}$
46	582.54	53.95	$1.94 \times 10^{11}$	83	1,168.25	73.98	$1.32 \times 10^{12}$	120	2,069.63	82.78	$5.14 \times 10^{12}$

<sup>a</sup> Reactions are based on point bearing at span ends.

<sup>b</sup> To obtain deflection for one wheel line in inches, divide the deflection coefficient by  $EI$  ( $\text{lb-in}^2$ ).

Table 16-8. - Maximum vehicle moment, reaction, and deflection coefficient. Simple span, one wheel line, impact factor not included (*continued*).

Vehicle type L90

Span (ft)	Moment (ft-kips)	Reaction <sup>a</sup> (kips)	Deflection <sup>b</sup> coefficient	Span (ft)	Moment (ft-kips)	Reaction <sup>a</sup> (kips)	Deflection <sup>b</sup> coefficient	Span (ft)	Moment (ft-kips)	Reaction <sup>a</sup> (kips)	Deflection <sup>b</sup> coefficient
0	75.00	30.00	$3.60 \times 10^7$	47	888.75	75.64	$3.21 \times 10^{11}$	84	1,721.25	81.96	$1.89 \times 10^{12}$
11	90.75	33.00	$4.79 \times 10^7$	48	911.25	75.94	$3.42 \times 10^{11}$	85	1,743.75	82.06	$1.96 \times 10^{12}$
12	108.00	36.00	$6.22 \times 10^7$	49	933.75	76.22	$3.65 \times 10^{11}$	86	1,766.25	82.15	$2.03 \times 10^{12}$
13	126.75	39.00	$7.91 \times 10^7$	50	956.25	76.50	$3.88 \times 10^{11}$	87	1,788.75	82.24	$2.10 \times 10^{12}$
14	147.00	42.00	$9.88 \times 10^7$	51	978.75	76.76	$4.13 \times 10^{11}$	88	1,811.25	82.33	$2.18 \times 10^{12}$
15	168.75	45.00	$1.22 \times 10^8$	52	1,001.25	77.02	$4.38 \times 10^{11}$	89	1,833.75	82.42	$2.25 \times 10^{12}$
16	191.25	47.81	$8.81 \times 10^8$	53	1,023.75	77.26	$4.64 \times 10^{11}$	90	1,856.25	82.50	$2.33 \times 10^{12}$
17	213.75	50.29	$1.11 \times 10^{10}$	54	1,046.25	77.50	$4.92 \times 10^{11}$	91	1,878.75	82.58	$2.41 \times 10^{12}$
18	236.25	52.50	$1.37 \times 10^{10}$	55	1,068.75	77.73	$5.20 \times 10^{11}$	92	1,901.25	82.66	$2.49 \times 10^{12}$
19	258.75	54.47	$1.67 \times 10^{10}$	56	1,091.25	77.95	$5.50 \times 10^{11}$	93	1,923.75	82.74	$2.57 \times 10^{12}$
20	281.25	56.25	$2.00 \times 10^{10}$	57	1,113.75	78.16	$5.81 \times 10^{11}$	94	1,946.25	82.82	$2.66 \times 10^{12}$
21	303.75	57.86	$2.37 \times 10^{10}$	58	1,136.25	78.36	$6.12 \times 10^{11}$	95	1,968.75	82.89	$2.74 \times 10^{12}$
22	326.25	59.32	$2.78 \times 10^{10}$	59	1,158.75	78.56	$6.45 \times 10^{11}$	96	1,991.25	82.97	$2.83 \times 10^{12}$
23	348.75	60.65	$3.24 \times 10^{10}$	60	1,181.25	78.75	$6.79 \times 10^{11}$	97	2,013.75	83.04	$2.92 \times 10^{12}$
24	371.25	61.88	$3.74 \times 10^{10}$	61	1,203.75	78.93	$7.15 \times 10^{11}$	98	2,036.25	83.11	$3.02 \times 10^{12}$
25	393.75	63.00	$4.29 \times 10^{10}$	62	1,226.25	79.11	$7.51 \times 10^{11}$	99	2,058.75	83.18	$3.11 \times 10^{12}$
26	416.25	64.04	$4.88 \times 10^{10}$	63	1,248.75	79.29	$7.89 \times 10^{11}$	100	2,081.25	83.25	$3.20 \times 10^{12}$
27	438.75	65.00	$5.53 \times 10^{10}$	64	1,271.25	79.45	$8.27 \times 10^{11}$	101	2,103.75	83.32	$3.30 \times 10^{12}$
28	461.25	65.89	$6.23 \times 10^{10}$	65	1,293.75	79.62	$8.67 \times 10^{11}$	102	2,126.25	83.38	$3.40 \times 10^{12}$
29	483.75	66.72	$6.98 \times 10^{10}$	66	1,316.25	79.77	$9.09 \times 10^{11}$	103	2,148.75	83.45	$3.50 \times 10^{12}$
30	506.25	67.50	$7.79 \times 10^{10}$	67	1,338.75	79.93	$9.51 \times 10^{11}$	104	2,171.25	83.51	$3.61 \times 10^{12}$
31	528.75	68.23	$8.66 \times 10^{10}$	68	1,361.25	80.07	$9.95 \times 10^{11}$	105	2,193.75	83.57	$3.71 \times 10^{12}$
32	551.25	68.91	$9.59 \times 10^{10}$	69	1,383.75	80.22	$1.04 \times 10^{12}$	106	2,216.25	83.63	$3.82 \times 10^{12}$
33	573.75	69.55	$1.06 \times 10^{11}$	70	1,406.25	80.36	$1.09 \times 10^{12}$	107	2,238.75	83.69	$3.93 \times 10^{12}$
34	596.25	70.15	$1.16 \times 10^{11}$	71	1,428.75	80.49	$1.14 \times 10^{12}$	108	2,261.25	83.75	$4.04 \times 10^{12}$
35	618.75	70.71	$1.28 \times 10^{11}$	72	1,451.25	80.63	$1.18 \times 10^{12}$	109	2,283.75	83.81	$4.16 \times 10^{12}$
36	641.25	71.25	$1.39 \times 10^{11}$	73	1,473.75	80.75	$1.24 \times 10^{12}$	110	2,306.25	83.86	$4.27 \times 10^{12}$
37	663.75	71.76	$1.52 \times 10^{11}$	74	1,496.25	80.88	$1.29 \times 10^{12}$	111	2,328.75	83.92	$4.39 \times 10^{12}$
38	686.25	72.24	$1.65 \times 10^{11}$	75	1,518.75	81.00	$1.34 \times 10^{12}$	112	2,351.25	83.97	$4.51 \times 10^{12}$
39	708.75	72.69	$1.79 \times 10^{11}$	76	1,541.25	81.12	$1.40 \times 10^{12}$	113	2,373.75	84.03	$4.64 \times 10^{12}$
40	731.25	73.13	$1.94 \times 10^{11}$	77	1,563.75	81.23	$1.45 \times 10^{12}$	114	2,396.25	84.08	$4.76 \times 10^{12}$
41	753.75	73.54	$2.10 \times 10^{11}$	78	1,586.25	81.35	$1.51 \times 10^{12}$	115	2,418.75	84.13	$4.89 \times 10^{12}$
42	776.25	73.93	$2.26 \times 10^{11}$	79	1,608.75	81.46	$1.57 \times 10^{12}$	116	2,441.25	84.18	$5.02 \times 10^{12}$
43	798.75	74.30	$2.43 \times 10^{11}$	80	1,631.25	81.56	$1.63 \times 10^{12}$	117	2,463.75	84.23	$5.15 \times 10^{12}$
44	821.25	74.66	$2.61 \times 10^{11}$	81	1,653.75	81.67	$1.69 \times 10^{12}$	118	2,486.25	84.28	$5.28 \times 10^{12}$
45	843.75	75.00	$2.80 \times 10^{11}$	82	1,676.25	81.77	$1.76 \times 10^{12}$	119	2,508.75	84.33	$5.42 \times 10^{12}$
46	866.25	75.33	$3.00 \times 10^{11}$	83	1,698.75	81.87	$1.82 \times 10^{12}$	120	2,531.25	84.38	$5.56 \times 10^{12}$

<sup>a</sup> Reactions are based on point bearing at span ends.

<sup>b</sup> To obtain deflection for one wheel line in inches, divide the deflection coefficient by EI (lb-in<sup>3</sup>).

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**Table 16-9. - Timber industry abbreviations.\***

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ACA	Ammoniacal copper arsenite	CIF	Cost, insurance, and freight
ACC	Acid copper chromate	CIFE	Cost, insurance, freight, and exchange
AD	Air-dried	CLF	Hundred lineal feet
ADF	After deducting freight	CLG	Ceiling
ADI	After date of invoice	CLR	Clear
AF	Alpine fir	CM	Center matched
ALS	American Lumber Standard	COM	Common
AS	Ashes	CONST	Construction
AST	Anti-stain treated	CS	Caulking seam
AV	Average	CSG	Casing
AVG	Average	CU FT	Cubic feet
AW&L	All widths and lengths	CV	Center Vee
B/L	Bill of lading	CV1S	Center Vee on one side
B&B	B and better	CV2S	Center Vee on two sides
B&BTR	B and better	CWT	Hundredweight
B&S	Beams & stringers	D/S	Drop siding
B1S	Edge bead one side	D/SDG	Drop siding
B2S	Edge bead two sides	D&CM	Dressed and center matched
BC&2S	Edge and bead two sides	D&H	Dressed and headed
BD FT	Board feet	D&M	Dressed and matched
BD	Board	D&SM	Dressed and standard matched
BDL	Bundle	D1S	Surfaced one side
BE	Beech	D2S	Surfaced two sides
BEV	Beveled	D2S&CM	Dressed two sides and center matched
BH	Boxed heart	D2S&SM	Dressed two sides and standard matched
BI	Birch		
BL	Bill of lading	DB PART	Double beaded partition
BM	Board measure	DB CLG	Double beaded ceiling
BSND	Bright sapwood no defect	DB2S	Edge and center beads two sides
BTR	Better	DET	Double end trimmed
BW	Black walnut	DF	Douglas fir
C/L	Carload	DF-L	Douglas Fir-Larch
CB	Center beaded	DIM	Dimension
CB1S	Center bead on one side	DKG	Decking
CB2S	Center bead on two sides	DS	Drop siding
CC	Cubical content	DV1S	Edge and center Vee one side
CCA	Chromated copper arsenate	DV2S	Edge and center Vee two sides
CF	Cost and freight	E	Edge
CFT	Cubic foot	E&CB1S	Edge and center bead one side
CG2E	Center groove on two edges	E&CB2S	Edge and center bead two sides

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\*Capitalization and punctuation of abbreviations may vary.

**Table 16-9. - Timber industry abbreviations (*continued*).**

E&CV1S	Edge and center Vee one side	J&P	Joists and planks
E&CV2S	Edge and center Vee two sides	JP	Jack pine
EB1S	Edge bead one side	JTD	Jointed
EB2S	Edge bead two sides	KD	Kiln dried
EE	Eased edges	L	Western larch
EG	Edge grain	L	Longer
EM	End matched	LBR	Lumber
ES	Engelmann spruce	LCL	Less than carload
EV1S	Edge Vee one side	LF	Light framing
EV2S	Edge Vee two sides	LFT	Linear feet
FA	Facial area	LFVC	Loaded fully visual capacity
FAC	Factory	LGR	Longer
FAS	Firsts and seconds	LGTH	Length
FAS1F	Firsts and seconds one face	LIN	Lineal
FBM	Feet board measure	LIN FT	Linear feet
FCPW	Flat car paper wrapped	LL	Long leaf
FG	Flat or slash grain	LNG	Lining
FJ	Finger joint	LP	Lodgepole pine
FLG	Flooring	LVL	Laminated lumber veneer
FOB	Freight on board	M	Thousand
FOHC	Free of heart center	M-S	Mixed species
FOK	Free of knots	MA	Maple
FRM	Framing	MBF	Thousand board feet
FRT	Freight	MBM	Thousand feet board measure
FT SM	Feet surface measure	MC	Moisture content
G	Girth	MERCH	Merchantable
G/R	Grooved roofing	MFT	Thousand feet
G/S	Gradestamped	MG	Mixed grain
GM	Grade marked	MG	Medium grain
H OR M	Hit or miss	MIN	Minimum
H-F	Hem-Fir	ML	Mixed lengths
H&M	Hit and miss	MLDG	Moulding
HB	Hollow back	MOE	Modulus of elasticity
HEM	Hemlock	MOR	Modulus of rupture
HI	Hickory	MSR	Machine stress rated
HRT	Heart	N	Nosed
HRT G	Heart girth	N1E	Nosed one edge
HRT FA	Heart facial area	N2E	Nosed two edges
HRT CC	Heart cubical content	NBM	Net board measure
IC	Incense cedar	NO	Number
IND	Industrial	NP	Red pine (northern)
IWP	Idaho white pine	OA	Oak

**Table 16-9. -Timber industry abbreviations (*continued*).**

OG	Ogee	S2S1E	Surfaced two sides, one edge
ORD	Order	S4S	Surfaced four sides
P&T	Posts and timbers	S4S&CS	Surfaced four sides and caulking
P1S	Planed (surfaced) one side	S4SEE	Surfaced four sides, eased edges
P2S	Planed (surfaced) two sides	SB1S	Single bead one side
PAD	Partially airdry	SB2S	Edge bead two sides
PART	Partition	SDG	Siding
PAT	Pattern	SE	Squared edge
PC	Piece	SE&S	Square edge and sound
PCS	Pieces	SEL	Select
PE	Plain end	SG	Slash or flat grain
PET	Precision end trimmed	SGSSND	Sapwood, gum spots and streaks, no defect
PO	Purchase order	SIT SPR	Sitka Spruce
PP	Ponderosa pine	SL	Shiplap
PW	Paper wrapped	SL&C	Shipper's load and count
QC	Quality control	SM	Surface measure
R/L	Random lengths	SM	Standard matched
R/S	Resawn	SP	Sugar pine
<b>R/W</b>	Random widths	SP	Southern Pine
RC	Red cedar	SPECS	Specifications
RDM	Random	SQ	Square
REG	Regular	SQRS	Squares
RES	Resawn	SR	Stress rated
RGH	Rough	SS	Sitka Spruce
RL	Random lengths	SSND	Sap stain no defect (stained)
RW	Redwood	STD	Standard
RW	Random widths	STD M	Standard matched
RW&L	Random lengths and widths	STK	Stock
S-Dry	Surfaced dry	STND	Stained
S-GRN	Surfaced green	STPG	Stepping
S/LAP	Shiplap	STR	Structural
S&E	Side & edge	STRUC	Structural
S1E	Surfaced one edge	STRUCT	Structural
S1S	Surfaced one side	SV1S	Edge Vee one side
S1S&CM	Surfaced one side and center matched	SV2S	Edge Vee two sides
S1S1E	Surfaced one side and one edge	SYP	Southern yellow pine
S1S2E	Surfaced one side and two edges	T&G	Tongued and grooved
S2E	Surfaced two edges	T&T	Truck and trailer
S2S	Surfaced two sides	TAD	Thoroughly air dried
S2S&CM	Surfaced two sides and center matched	TBR	Timber
S2S&SL	Surfaced two sides and shiplapped	UTIL	Utility
S2S&SM	Surfaced two sides and standard matched		

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**Table 16-9. - Timber industry abbreviations (*continued*).**

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V&CV1S	Edge and center Vee one side	WHAD	Worm holes a defect
V&CV2S	Edge and center Vee two sides	WHND	Worm holes no defect
V1S	Edge Vee one side	WP	Ponderosa pine
V2S	Edge Vee two sides	WRC	Western redcedar
VG	Vertical (edge) grained	WRD	Western redcedar
WC	Western redcedar	WT	Weight
WCH	West Coast hemlock	WTH	Width
WCW	West Coast woods	WW	White woods
WDR	Wider	YC	Alaska yellow cedar
WF	Western fir or White fir	YP	Yellow pine

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**Table 16-10. - List of institutes, agencies, and industry associations.**

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American Association of State Highway and  
Transportation Officials (AASHTO)  
444 North Capitol Street NW, Suite 225  
Washington, DC 20001

American Consulting Engineers Council (ACEC)  
1015 Fifteenth Street NW, #802  
Washington, DC 20005  
(202) 347-7474

American Forest Institute (AFI)  
1619 Massachusetts Avenue NW  
Washington, DC 20036

American Institute of Architects (AIA)  
1735 New York Avenue NW  
Washington, D.C. 20006  
(202) 626-7300

American Institute of Timber Construction (AITC)  
11818 SE Mill Plaine Blvd, Suite 415  
Vancouver, WA 98684  
(206) 254-9132

American Lumber Standards Committee (ALSC)  
P.O. Box 210  
Germantown, MD 20874  
(301) 972-1700

American National Standards Institute (ANSI)  
1430 Broadway  
New York, NY 10018  
(212) 642-4972

American Plywood Association (APA)  
P.O. Box 11700  
Tacoma, WA 98411  
(206) 565-6600

American Society for Testing and Materials (ASTM)  
1916 Race Street  
Philadelphia, PA 19103  
(215) 299-5400

American Society of Civil Engineers (ASCE)  
345 East 47th Street  
New York, NY 10017  
(212) 705-7490

American Wood Council (AWC)  
1250 Connecticut Avenue NW, Suite 230  
Washington, DC 20036  
(202) 833-1595

American Wood Preservers Bureau (AWPB)  
P.O. Box 5283  
Springfield, VA 22150  
(703) 339-6660

American Wood Preservers Institute (AWPI)  
1945 Gallows Road, Suite 405  
Vienna, VA 22180  
(703) 893-4005

American Wood Preservers' Association (AWPA)  
P.O. Box 849  
Stevensville, MD 21666  
(301) 643-4163

Associated General Contractors (AGC)  
1957 East Street NW  
Washington, DC 20006  
(202) 393-2040

California Redwood Association (CRA)  
591 Redwood Highway, Suite 3100  
Mill Valley, CA 94941  
(415) 381-1304

Canadian Wood Council (CWC)  
85 Albert St.  
Ottawa, ON, Canada K1P 6A4  
(613) 235-7221

Construction Specifications Institute (CSI)  
601 Madison Street  
Alexandria, VA 22314  
(703) 684-0300

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**Table 16-10. - List of institutes, agencies, and industry associations (*continued*).**

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Forest Products Laboratory (FPL) U.S. Department of Agriculture One Gifford Pinchot Drive Madison, WI 53705-2398 (608) 231-9200	National Timber Piling Council, Inc. (NTPC) P.O. Box 358 Fords, NJ 08863 (201) 738-8811
Forest Products Research Society (FPRS) 2801 Marshall Court Madison, WI 53705 (608) 231-1361	North American Wholesale Lumber Association (NAWLA) 2340 South Arlington Heights Road, Suite 680 Arlington Heights, IL 60005 (312) 981-8630
National Bureau of Standards (NBS) U.S. Department of Commerce Washington, DC 20234	North West Timber Association (NWTa) 1355 Oak Street, Suite D P.O. Box 5554 Eugene, OR 97405 (503) 686-9603
Ministry of Transportation and Communications Research and Development Branch Room 331, Central Building, Third Floor 1201 Wilson Avenue Downsview, ON, Canada M3M 1J8 (416) 235-4700	Northeastern Lumber Manufacturers Association (NELMA) 4 Fundy Road Falmouth, ME 04105 (207) 781-2252
National Forest Products Association (NFPA) 1250 Connecticut Avenue NW Washington, DC 20036 (202) 463-2700	Redwood Inspection Service (RIS) 591 Redwood Highway, Suite 3100 Mill Valley, CA 94941 (415) 381-1304
National Hardwood Lumber Association (NHLA) P.O. Box 34518 Memphis, TN 38134 (901) 377-1818	Society of American Wood Preservers, Inc. 7297 Lee Highway-Unit P Falls Church, VA 22042 (703) 237-0900
National Institute of Building Science (NIBS) 1015 Fifteenth Street NW, Suite 700 Washington, DC 20006	Southern Forest Products Association (SFPA) P.O. Box 52468 New Orleans, LA 70152 (504) 443-4464
National Lumber Grades Authority (NLGA) P.O. Box 97 Ganges, BC, Canada VDS 1E0	Southern Pine Inspection Bureau (SPIB) 4709 Scenic Highway Pensacola, FL 32504-9094 (904) 434-2611
National Technical Information Service (NTIS) US. Department of Commerce 5285 Port Royal Road Springfield, VA 22161	

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**Table 16-10. - List of institutes, agencies, and industry associations (*continued*).**

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Truss Plate Institute (TPI) 583 D'Onofrio Drive, Suite 200 Madison, WI 53719 (608) 833-5900	Western Wood Preservers Institute 1499 Bayshore Highway, Suite 208 Burlingame, CA 94010 (415) 692-0958
West Coast Lumber Inspection Bureau (WCLIB) 6980 SW Varnes Road P.O. Box 23145 Portland, OR 97223 (503) 639-0651	Western Wood Products Association (WWPA) 1500 Yeon Building Portland, OR 97204 (503) 224-3930
Western Red Cedar Lumber Association (WRCLA) 1500 Yeon Building Portland, OR 97204 (503) 224-3930	Wood Truss Council of America (NTCA) 111 Wacker Drive Chicago, IL 60601 (312) 644-6601

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**Table 16-11. - Partial list of firms and plants equipped to produce structural glulam.<sup>a</sup>**

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Alamco Wood Products, Inc.  
1410 West 9th Street  
Albert Lea, MN 56007  
(507) 373-1401

American Laminators, Inc.  
P.O. Box 1846  
Eugene, OR 97440  
(503) 345-7777  
Laminating plant locations:  
Drain, OR 97435  
Swisshome, OR 97480

Anthony Forest Products Company  
Laminating Division  
P.O. Box 1877  
El Dorado, AR 71730  
(501) 862-5594

Bohemia, Inc.  
P.O. Box 1819  
Eugene, OR 97401  
(503) 342-6262

Boise Cascade Corporation  
P.O. Box 50  
Boise, ID 83728  
(208) 384-7151

Unit Structures, Inc.  
P.O. Box 23215  
Louisville, KY 97479  
(502) 244-0825  
Laminating plant locations:  
Magnolia, AR 71753  
Morrisville, NC 27560

Laminated Technologies Inc.  
P.O. Box 69  
Magna, UT 84044  
(801) 250-1585

Laminated Timbers, Inc.  
P.O. Box 788  
London, KY 40741  
(606) 864-5134

Laminated Wood Products Company  
P.O. Box L  
Ontario, OR 97914  
(503) 889-5357

Mississippi Laminators  
P.O. Box 405  
Shubuta, MS 39360  
(601) 687-1571

QB Corporation  
P.O. Box 1647  
Salmon, ID 83467  
(208) 756-4248

Riddle Laminators  
P.O. Box 66  
Riddle, OR 97469  
(503) 874-3151

Rosboro Lumber Company  
P.O. Box 20  
Springfield, OR 97477  
(503) 746-8411

Sentinel Structures, Inc.  
477 South Peck Avenue  
Peshtigo, WI 54157  
(715) 582-4544

Shelton Structures, Inc.  
P.O. Box 237  
Shelton, WA 98584  
(206) 426-5488

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<sup>a</sup>This list is based on information current at the time of publication and may be incomplete. Inclusion of firm names implies no endorsement as to quality or prices.

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**Table 16-11. -Partial list of firms and plants equipped to produce structural glulam *(continued)*.**

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Southern Laminators, Inc.  
P.O. Box 1062  
Denham Springs, LA 70726  
(504) 664-3359

Standard Structures, Inc.  
P.O. Box K  
Santa Rosa, CA 95402  
(707) 544-2982

Structural Wood Systems, Inc.  
P.O. Box 250  
Greenville, AL 36037  
(205) 382-6534

Timberweld Manufacturing  
P.O. Box 1535  
Billings, MT 59103  
(406) 252-7119

Timfab, Inc.  
P.O. Box 7  
Clackamas, OR 97015  
(503) 656-1668

Tyee Timbers, Inc.  
P.O. Box 308  
Sutherlin, OR 97479  
(503) 459-5384

Unadilla Laminated Products  
Unadilla, NY 13849  
(607) 369-9341

Weyerhaeuser Company  
Tacoma, WA 98477  
(206) 924-2345  
Laminating plant location:  
Cottage Grove, OR 97424

Wood Fabricators, Inc.  
Iron Horse Park  
North Billerica, MA 01862  
(617) 663-6511

**Table 16-12. - Partial list of suppliers of pressure-treated wood for bridge construction.**

The following list of suppliers of pressure treated wood was compiled from responses received from a questionnaire distributed by the American Wood Preservers Institute and the Society of American Wood Preservers, Inc. To simplify use, the list has been prepared by geographic regions identified on the map below. These regions are based on marketing areas identified through the questionnaire. For more current information, contact one of the national wood preserving associations given in Table 16-10.

Inclusion of a company name in this listing is for informational purposes only and implies no endorsement as to price or quality.



Company name	Geographic region(s)
Alabama/Georgia Wood Preserving Co. P.O. Drawer 9 Lafayette, AL 36862 (205) 864-9303 CCA	Southeast, Midwest, Southeast
Allweather Wood Treaters, Inc. P.O. Box 227 Washougal, WA 98671 (206) 835-8547 CCA	Southwest, Rocky Mountain, West Coast

**Table 16-12. - Partial list of suppliers of pressure-treated wood for bridge construction *(continued)*.**

<b>Company name</b>	<b>Geographic region(s)</b>
Atlantic Wood Industries, Inc. P.O. Box 1608 Savannah, GA 31402 (912) 964-1234 CCA, Creosote & Penta	Northeast, Middle Atlantic, Southeast, Midwest, Southcentral, Northcentral
Ayres & Baker Pole & Post Co. P.O. Box 610 Mt. View, WY 82939 (307) 782-3170 CCA	Southwest, Rocky Mountain
J.H. Baxter & Company P.O. Box 10797 Eugene, OR 97440 (503) 689-3020 ACZA, Creosote & Penta	Nationwide
Cherokee Wood Preservers, Inc. P.O. Box 68 Mosheim, TN 37818 (615) 422-4131 CCA	Middle Atlantic, Southeast, Midwest, Southcentral
Colfax Creosoting Company P.O. Box 231 Pineville, LA 71361 (318) 442-2467 CCA, Creosote & Penta	Nationwide
Conasauga River Lumber Co. P.O. Box 2 Conasauga, TN 37316 (615) 338-2886 CCA	Southeast, Southcentral
Conrad Lumber Company 3998 Wildwood Dr. North Bend, OR 97459 (503) 756-2595 CCA	Rocky Mountain, West Coast.

**Table 16-12. - Partial list of suppliers of pressure-treated wood for bridge construction *(continued)*.**

<b>Company name</b>	<b>Geographic region(s)</b>
Continental Wood Preservers, Inc. 7500 E. Division Detroit, MI 48212 (313) 365-4200 CCA	Midwest
Fernwood Industries P.O. Box 90 Fernwood, MS 39635 (601) 684-2011 Creosote & Penta	Southcentral, Northcentral, Southwest
Follen Wood Preserving Co., Inc. P.O. Box 8121 Jackson, MS 39204 (601) 948-1746 CCA	Southeast, Southcentral
Fontana Wholesale Lumber, Inc. P.O. Box 1070 Fontana, CA 92335 (714) 350-1214 CCA	Southwest, Rocky Mountain, West Coast
Frontier Lumber Co., Inc. 1941 Elmwood Ave. Buffalo, NY 14207 (716) 873-8500 CCA	Middle Atlantic
Great Southern Wood Preservers P.O. Box 458 Abbeville, AL 36310 (205) 585-2291 CCA	Southeast, Southcentral
Green Bay Wood Preserving P.O. Box 194 Sheboygan Falls, WI 53085 (414) 467-2671 CCA	Midwest

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**Table 16-12. - Partial list of suppliers of pressure-treated wood for bridge construction *(continued)*.**

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<b>Company name</b>	<b>Geographic region(s)</b>
Hatheway & Patterson Co., Inc. 15 County St., Box 177 Mansfield, MA 02048 (617) 339-8934 CCA & Penta	Northeast, Middle Atlantic
Hoover Treated Wood Products P.O. Box 746 Thomson, GA 30824 (800) 832-9663 CCA	Northeast, Middle Atlantic, Southeast, Midwest, Northcentral, Southcentral
Hughes Brothers, Inc. P.O. Box 159 Seward, NE 68434 (402) 643-2991 Penta	Nationwide
Jasper Wood Treating, Inc. P.O. Box 106 Jasper, OR 97438 (800) 331-0656 CCA	Southwest, Rocky Mountain, West Coast
Koppers Industries 436 7th Avenue Pittsburgh, PA 15219-1800 (412) 227-2001 CCA, Creosote & Penta	Nationwide
Land O'Lakes Wood Preserving P.O. Box 87 Tenstrike, MN 56683 (218) 586-2203 CCA	Midwest, Northcentral
Langdale Forest Products Co. P.O. Box 1088 Valdosta, GA 31603 (912) 242-7450 CCA	Northeast, Middle Atlantic, Southeast, Midwest, Southcentral

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**Table 16-12. - Partial list of suppliers of pressure-treated wood for bridge construction *(continued)*.**

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<b>Company name</b>	<b>Geographic region(s)</b>
L.L. Brewton Lumber Co. P.O. Box 191 Winnfield, LA 71483 (318) 628-4131 CCA	Southcentral, Southwest
The Maine Wood Treaters, Inc. RFD 1, Box 5130 Mechanic Falls, ME 04356 (207) 345-8411 CCA	Northeast
McArthur Lumber & Post Co., Inc State Route 93N McArthur, OH 45651 (614) 596-5880 CCA	Midwest, Southcentral
McCormick & Baxter Creosoting P.O. Box 3048 Portland, OR 97208 (503) 286-8394 ACZA, Creosote & Penta	West Coast
McFarland Cascade P.O. Box 1496 Tacoma, WA 98401 (800) 426-8430 ACZA, CCA, Creosote & Penta	Nationwide
T.R. Miller Mill Co. Inc. P.O. Box 708 Brewton, AL 36427 CCA, Creosote & Penta (205) 867-4331	Northeast, Middle Atlantic, Southeast, Midwest, Southcentral, Northcentral
Morgan Lumber Company, Inc. P.O. Drawer 309 Marshville, NC 28103 (704) 624-2146 CCA	Southeast

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**Table 16-12. - Partial list of suppliers of pressure-treated wood for bridge construction *(continued)*.**

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<b>Company name</b>	<b>Geographic region(s)</b>
National Wood Preservers, Inc. P.O. Box F Havertown, PA 19083 (215) 528-6490 CCA	Northeast, Middle Atlantic
Niedermeyer-Martin Co. P.O. Box 3768 Portland, OR 97208 (800) 547-6952 CCA, Creosote & Penta	Nationwide
Pacific Wood Preserving of Bakersfield 5601 District Blvd. Bakersfield, CA 93313 (805) 833-0429 CCA, Creosote	Southwest, Rocky Mountain, West Coast
Permapost Products Company P.O. Box 100 Hillsboro, OR 97123 (800) 828-0222 CCA & Penta	Nationwide
Pressure Treating Timber Co. 3200 Gowen Rd. Boise, ID 83705 (208) 343-6456 Penta	Southwest, Rocky Mountain, West Coast
Seaman Timber Co., Inc. P.O. Box 372 Montevallo, AL 35115 (205) 665-2536 CCA & Creosote	Southeast, Southcentral, Midwest, Southwest
Selma Treating Co. P.O. Box 89 Selma, CA 93662 (209) 896-1234 CCA & Penta	Southwest, Rocky Mountain, West Coast

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**Table 16-12. - Partial list of suppliers of pressure-treated wood for bridge construction *(continued)*.**

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<b>Company name</b>	<b>Geographic region(s)</b>
Southern Wood Piedmont P.O. Box 5447 New South Park Spartanburg, SC 29304 (803) 576-7660 CCA, Creosote & Penta	Northeast, Southeast, Middle Atlantic, Midwest
Straits Wood Preserving, Inc. P.O. Box 316 Grayling, MI 49738 (517) 348-2893 CCA	Midwest
Straits Wood Treating, Inc. 610 Oak St. Tawas City, MI 48763 (800) 292-1158 ext.280 CCA	Midwest
Swift Lumber, Inc. P.O. Drawer 1298 Atmore, AL 36504 (205) 368-8800 CCA	Southeast, Southcentral
Taylor-Ramsey Corp. P.O. Box 11888 Lynchburg, VA 24506 (804) 846-6571 CCA	Northeast, Middle Atlantic, Southeast, Southcentral, Midwest
Universal Forest Products P.O. Box 129 Granger, IN 46530 (219) 277-7670 CCA	Midwest
Universal Forest Products P.O. Box 31 Gordon, PA 17936 (717) 875-2811 CCA	Middle Atlantic

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**Table 16-12. - Partial list of suppliers of pressure-treated wood for bridge construction *(continued)*.**

<b>Company name</b>	<b>Geographic region(s)</b>
Universal Forest Products 1118 Humes Road Janesville, WI 53545 (608) 755-6200 CCA	Midwest
Western Wood Preserving Co. P.O. Box L Sumner, WA 98390 (206) 863-8191 CCA	West Coast
Weyerhaeuser Company Tacoma, WA 98477 (206) 924-3630 Creosote & Penta	Nationwide
Wheeler Consolidated, Inc. P.O. Box 26100 St. Louis Park, MN 55426 (612) 929-7854 CCA, Creosote & Penta	Nationwide
Wigland Corp. 850 Elkton Dr. Colorado Springs, CO 80907 (303) 599-8838 CCA	Northcentral, Southwest, Rocky Mountain
Wood Preservers, Inc. P.O. Box 1018 Warsaw, VA 22572 (804) 333-4022 CCA & Creosote	Northeast, Southeast, Middle Atlantic
Wyckoff Company 1508 Peoples Bank Bldg. Seattle, WA 98171 (206) 624-3535 ACZA, Creosote & Penta	Nationwide

# CREOSOTE PRESSURE-TREATED WOOD

## CONSUMER INFORMATION

This wood has been preserved by pressure treatment with an EPA-registered pesticide containing creosote to protect it from insect attack and decay. Wood treated with creosote should be used only where such protection is important.

Creosote penetrates deeply into and remains in the pressure-treated wood for a long time. Exposure to creosote may present certain hazards. Therefore, the following precautions should be taken both when handling the treated wood and in determining where to use the treated wood.

## USE SITE PRECAUTIONS

Wood treated with creosote should not be used where it will be in frequent or prolonged contact with bare skin (for example, chairs and other outdoor furniture) unless an effective sealer has been applied.

Creosote-treated wood should not be used in residential interiors. Creosote-treated wood in interiors of industrial buildings should be used only for industrial building components which are in ground contact and are subject to decay or insect infestation and wood block flooring. For such uses, two coats of an appropriate sealer must be applied. Sealers may be applied at the installation site.

Wood treated with creosote should not be used in the interiors of farm buildings where there may be direct contact with domestic animals or livestock which may crib (bite) or lick the wood.

In interiors of farm buildings where domestic animals or livestock are unlikely to crib (bite) or lick the wood, creosote-treated wood may be used for building components which are in ground contact and are subject to decay or insect infestation if two coats of an effective sealer are applied. Sealers may be applied at the installation site.

Do not use creosote-treated wood for farrowing or brooding facilities.

Do not use treated wood under circumstances where the preservative may become a component of food or animal feed. Examples of such use would be structures or containers for storing silage or food.

Do not use treated wood for cutting boards or countertops.

Only treated wood that is visibly clean and free of surface residues should be used for patios, decks and walkways.

Do not use treated wood for construction of those portions of beehives which may come into contact with the honey.

Creosote-treated wood should not be used where it may come into direct or indirect contact with public drinking water, except for uses involving incidental contact such as docks and bridges.

Do not use creosote-treated wood where it may come into direct or indirect contact with drinking water for domestic animals or livestock, except for uses involving incidental contact such as docks and bridges.

## HANDLING PRECAUTIONS

Dispose of treated wood by ordinary trash collection or burial. Treated wood should not be burned in open fires or in stoves, fireplaces, or residential boilers, because toxic chemicals may be produced as part of the smoke and ashes. Treated wood from commercial or industrial use (e.g., construction sites) may be burned only in commercial or industrial incinerators or boilers in accordance with state and Federal regulations.

Avoid frequent or prolonged inhalation of sawdust from treated wood. When sawing and machining treated wood, wear a dust mask. Whenever possible, these operations should be performed outdoors to avoid indoor accumulations of airborne sawdust from treated wood.

Avoid frequent or prolonged skin contact with creosote-treated wood; when handling the treated wood, wear long-sleeved shirts and long pants and use gloves impervious to the chemicals (for example, gloves that are vinyl-coated).

When power-sawing and machining, wear goggles to protect eyes from flying particles.

After working with the wood, and before eating, drinking, and use of tobacco products, wash exposed areas thoroughly.

If oily preservatives or sawdust accumulate on clothes, launder before reuse. Wash work clothes separately from other household clothing.

Coal tar pitch and coal tar pitch emulsion are effective sealers for creosote-treated wood-block flooring. Urethane, epoxy, and shellac are acceptable sealers for all creosote-treated wood.

# PENTACHLOROPHENOL PRESSURE-TREATED WOOD

## CONSUMER INFORMATION

This wood has been preserved by pressure-treatment with an EPA-registered pesticide containing pentachlorophenol to protect it from insect attack and decay. Wood treated with pentachlorophenol should be used only where such protection is important.

Pentachlorophenol penetrates deeply into and remains in the pressure-treated wood for a long time. Exposure to pentachlorophenol may present certain hazards. Therefore, the following precautions should be taken both when handling the treated wood and in determining where to use and dispose of the treated wood.

## USE SITE PRECAUTIONS

Logs treated with pentachlorophenol should not be used for log homes.

Wood treated with pentachlorophenol should not be used where it will be in frequent or prolonged contact with bare skin (for example, chairs and other outdoor furniture), unless an effective sealer has been applied.

Pentachlorophenol-treated wood should not be used in residential, industrial, or commercial interiors except for laminated beams or for building components which are in ground contact and are subject to decay or insect infestation and where two coats of an appropriate sealer are applied. Sealers may be applied at the installation site.

Wood treated with pentachlorophenol should not be used in the interiors of farm buildings where there may be direct contact with domestic animals or livestock which may crib (bite) or lick the wood.

In interiors of farm buildings where domestic animals or livestock are unlikely to crib (bite) or lick the wood, pentachlorophenol-treated wood may be used for building components which are in ground contact and are subject to decay or insect infestation and where two coats of an appropriate sealer are applied. Sealers may be applied at the installation site.

Do not use pentachlorophenol-treated wood for farrowing or brooding facilities.

Do not use treated wood under circumstances where the preservative may become a component of food or animal feed. Examples of such sites would be structures or containers for storing silage or food.

Do not use treated wood for cutting-boards or counter-tops.

Only treated wood that is visibly clean and free of surface residue should be used for patios, decks and walkways.

Do not use treated wood for construction of those portions of beehives which may come into contact with the honey.

Pentachlorophenol-treated wood should not be used where it may come into direct or indirect contact with public drinking water, except for uses involving incidental contact such as docks and bridges.

Do not use pentachlorophenol-treated wood where it may come into direct or indirect contact with drinking water for domestic animals or livestock, except for uses involving incidental contact such as docks and bridges.

## HANDLING PRECAUTIONS

Dispose of treated wood by ordinary trash collection or burial. Treated wood should not be burned in open fires or in stoves, fireplaces, or residential boilers because toxic chemicals may be produced as part of the smoke and ashes. Treated wood from commercial or industrial use (e.g., construction sites) may be burned only in commercial or industrial incinerators or boilers rated at 20 million BTU/hour or greater heat input or its equivalent in accordance with state and Federal regulations.

Avoid frequent or prolonged inhalation of sawdust from treated wood. When sawing and machining treated wood, wear a dust mask. Whenever possible, these operations should be performed outdoors to avoid indoor accumulations of airborne sawdust from treated wood.

Avoid frequent or prolonged skin contact with pentachlorophenol-treated wood; when handling the treated wood, wear long-sleeved shirts and long pants and use gloves impervious to the chemicals (for example, gloves that are vinyl-coated).

When power-sawing and machining, wear goggles to protect eyes from flying particles.

After working with the wood, and before eating, drinking, and use of tobacco products, wash exposed areas thoroughly.

If oily preservatives or sawdust accumulate on clothes, launder before reuse. Wash work clothes separately from other household clothing.

Urethane, shellac, latex epoxy enamel and varnish are acceptable sealers for pentachlorophenol-treated wood.

# INORGANIC ARSENICAL PRESSURE-TREATED WOOD

(Including: CCA, ACA, and ACZA)

## CONSUMER INFORMATION

This wood has been preserved by pressure-treatment with an EPA-registered pesticide containing inorganic arsenic to protect it from insect attack and decay. Wood treated with inorganic arsenic should be used only where such protection is important.

Inorganic arsenic penetrates deeply into and remains in the pressure-treated wood for a long time. Exposure to inorganic arsenic may present certain hazards. Therefore, the following precautions should be taken both when handling the treated wood and in determining where to use or dispose of the treated wood.

## USE SITE PRECAUTIONS

Wood pressure-treated with waterborne arsenical preservatives may be used inside residences as long as all sawdust and construction debris are cleaned up and disposed of after construction.

Do not use treated wood under circumstances where the preservative may become a component of food or animal feed. Examples of such sites would be structures or containers for storing silage or food.

Do not use treated wood for cutting-boards or counter-tops.

Only treated wood that is visibly clean and free of surface residue should be used for patios, decks and walkways.

Do not use treated wood for construction of those portions of beehives which may come into contact with the honey.

Treated wood should not be used where it may come into direct or indirect contact with public drinking water, except for uses involving incidental contact such as docks and bridges.

## HANDLING PRECAUTIONS

Dispose of treated wood by ordinary trash collection or burial. Treated wood should not be burned in open fires or in stoves, fireplaces, or residential boilers because toxic chemicals may be produced as part of the smoke and ashes. Treated wood from commercial or industrial use (e.g., construction sites) may be burned only in commercial or industrial incinerators or boilers in accordance with state and Federal regulations.

Avoid frequent or prolonged inhalation of sawdust from treated wood. When sawing and machining treated wood, wear a dust mask. Whenever possible, these operations should be performed outdoors to avoid indoor accumulations of airborne sawdust from treated wood.

When power-sawing and machining, wear goggles to protect eyes from flying particles.

After working with the wood, and before eating, drinking, and use of tobacco products, wash exposed areas thoroughly.

If preservatives or sawdust accumulate on clothes, launder before reuse. Wash work clothes separately from other household clothing.

Approved by the U.S. Environmental Protection Agency

7-85

Figure 16-3—Consumer information sheet for inorganic arsenical pressure-treated wood.